

# PASS/EQUIP Nozzle-FEM Overview Webinar

Powerful software for nozzle-to-shell junctions analysis

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PIPING AND EQUIPMENT  
ANALYSIS & SIZING SUITE

# PASS Suite

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The PASS software tools provide smart simulation & sizing tools for every piping and equipment engineer /designer



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# Company Overview

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- > 50 years history
- > 3,000 active users worldwide
- Best in class modern methods, algorithms and software libraries
- Embedded knowledge and support/training from industry experts
- User-friendly interface and flexible CAD integration
- Affordable price and flexible licensing



# PASS Suite Users



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## PASS/Nozzle-FEM

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Powerful  
software for  
strength  
analysis of  
nozzle junction  
with wide  
capabilities

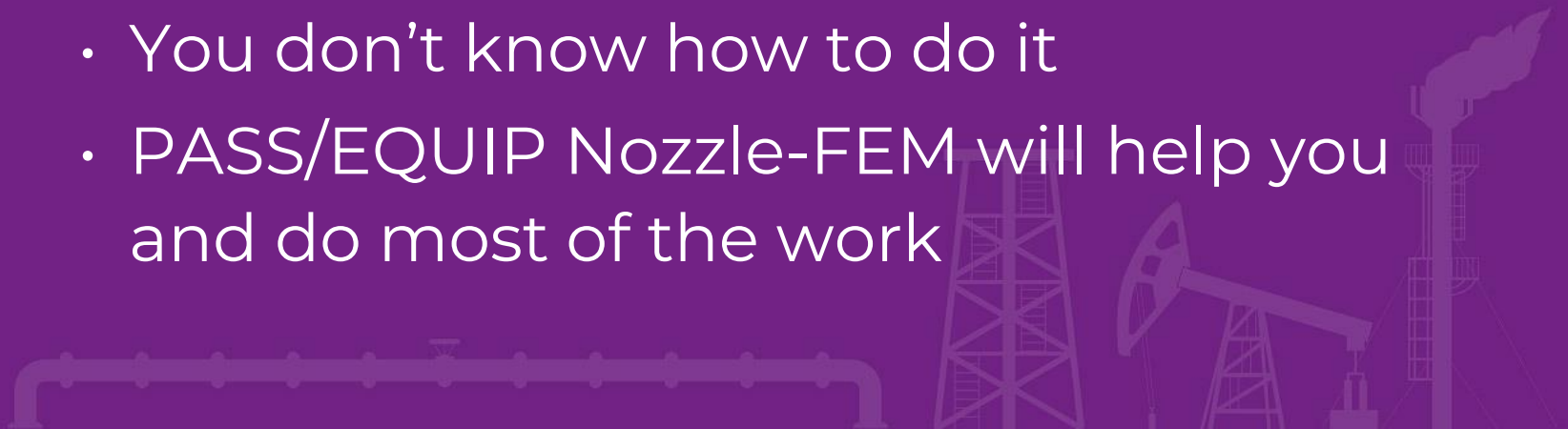


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## Why do you need Nozzle-FEM?

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- You design pressure vessel, piping or something similar
- You need to specify allowable loads and stiffness (flexibility) of nozzle junction
- You are a good and responsible engineer
- You need to estimate strength of nozzle junctions
- You don't know how to do it
- PASS/EQUIP Nozzle-FEM will help you and do most of the work



# Why do you need Nozzle-FEM?

There are several methods to solve this problem:

- Using an analytical approach as per industry standards, like WRC 107(537).
- Using of a complex universal CAE software, like ANSYS, NASTRAN, COSMOS, Abaqus, etc.
- Using of specialized software like PASS/Equip Nozzle-FEM.



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## Options

1. Industry standards:



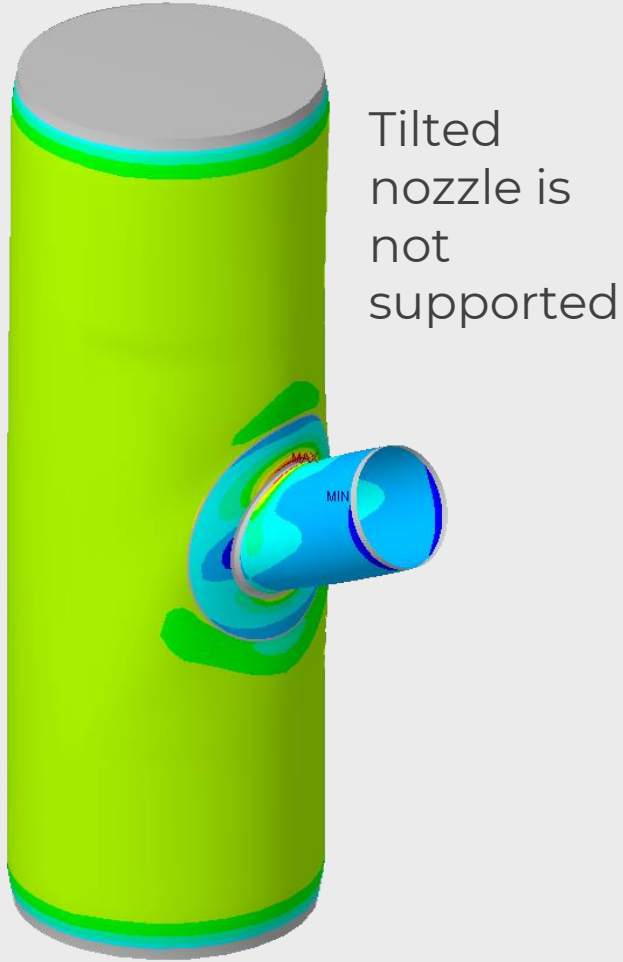
2. Universal CAE software:



3. Specialized software:



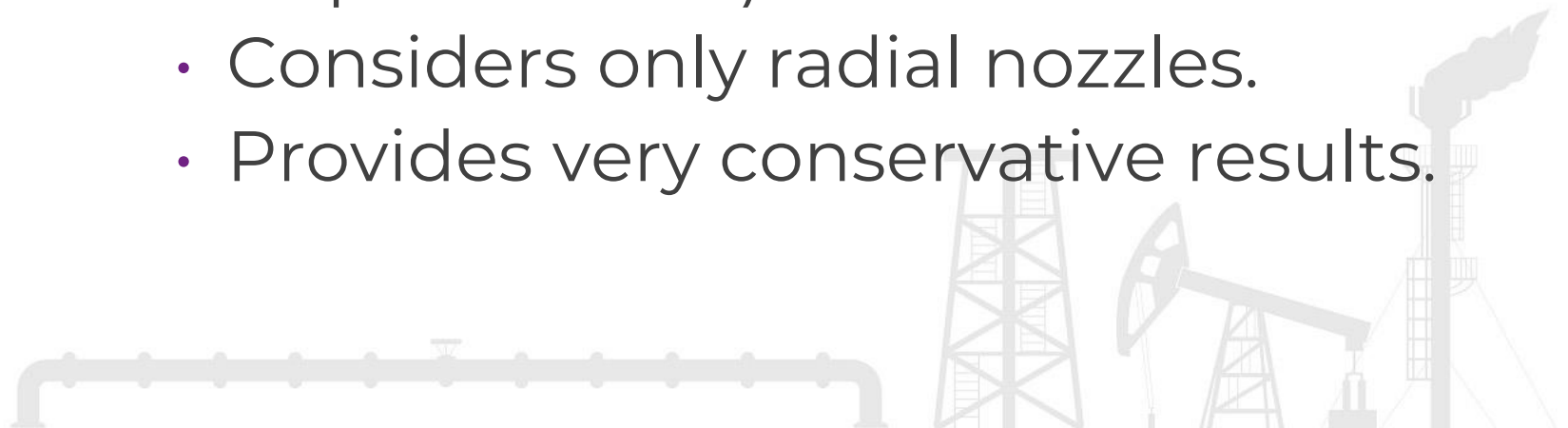
# Option 1



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# Analytical approach

- The most commonly used approach at present.
- Some analysis according to this approach is implemented in software like PASS/EQUIP Vessel.
- It has a number of disadvantages:
  - Limited variety of geometric shell shapes (mainly cylindrical and elliptical shells).
  - Considers only radial nozzles.
  - Provides very conservative results.





# Universal CAE

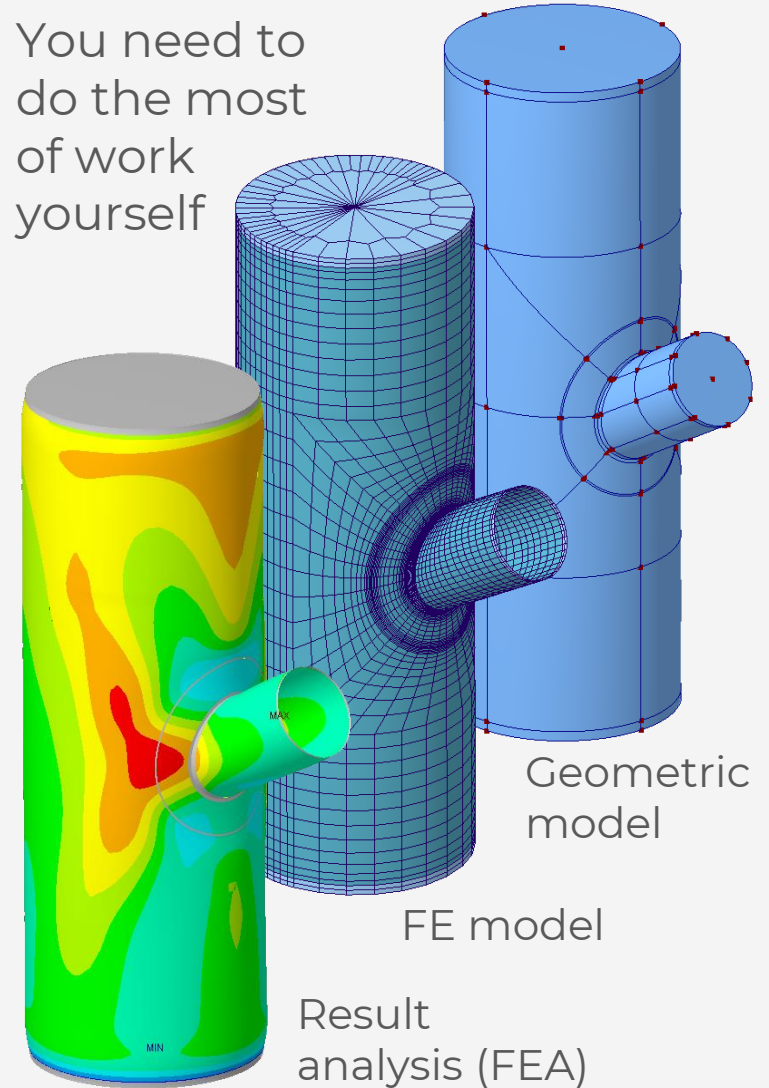
- It is great! But...
- Universal CAE software is very expensive
- You will have to do a lot of work yourself:
  - create a geometric model
  - create a finite-element model
  - handle calculation results
- Using of CAE software requires skills in different disciplines: surface and solid modeling, numerical methods (FEM) etc.



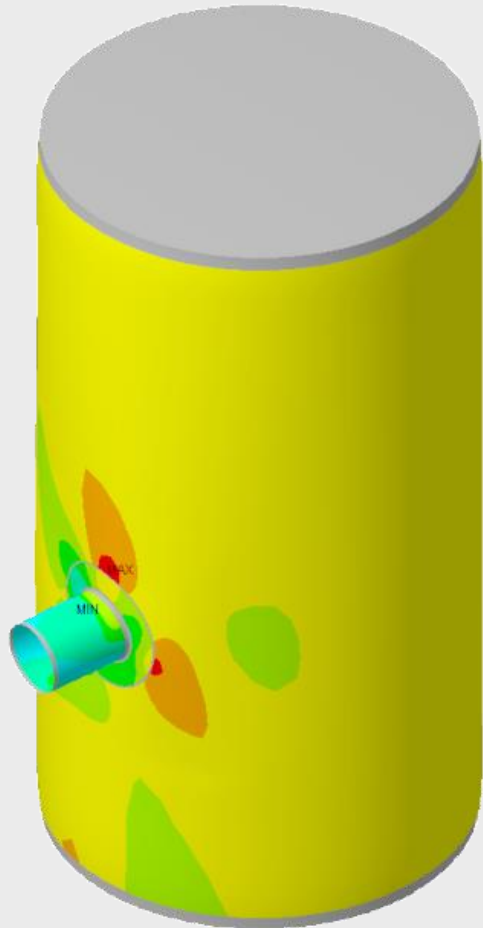
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## Option 2

You need to  
do the most  
of work  
yourself



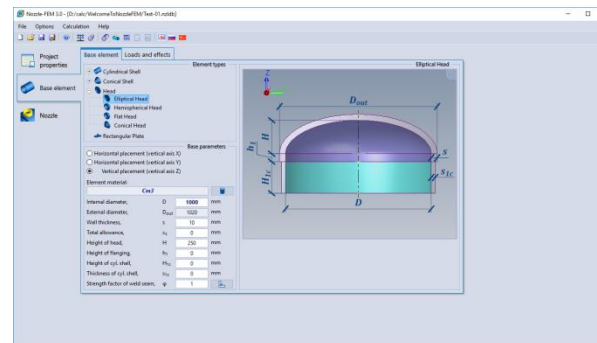
# Option 3



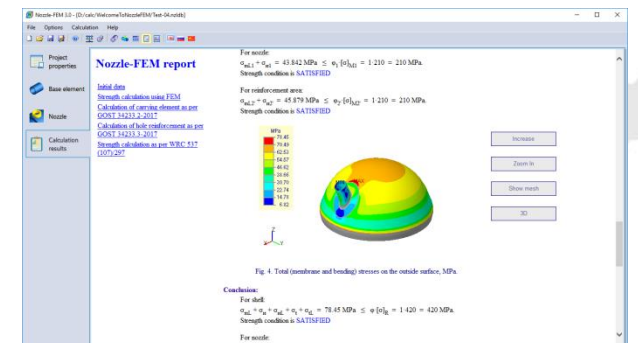
# Specialized software

- Supports a wide variety of shell and nozzle configurations.
- Doesn't require special knowledge and skills.
- Less time for calculation and decision making.

Object data  
(structural dimensions)



Result report



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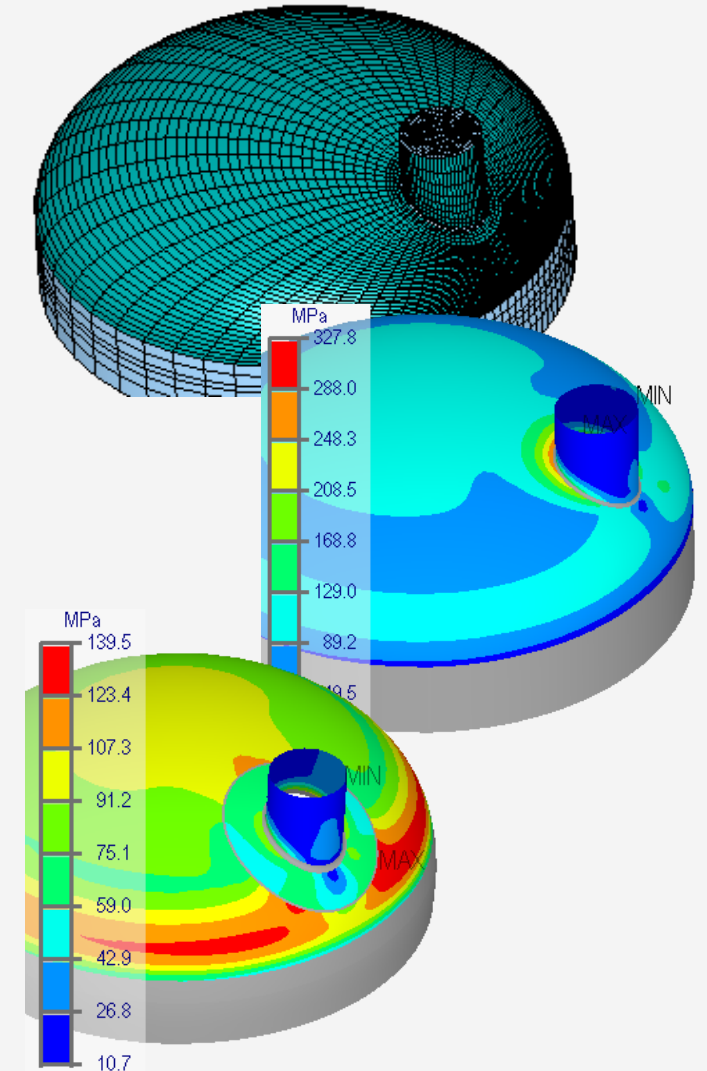
# Main features

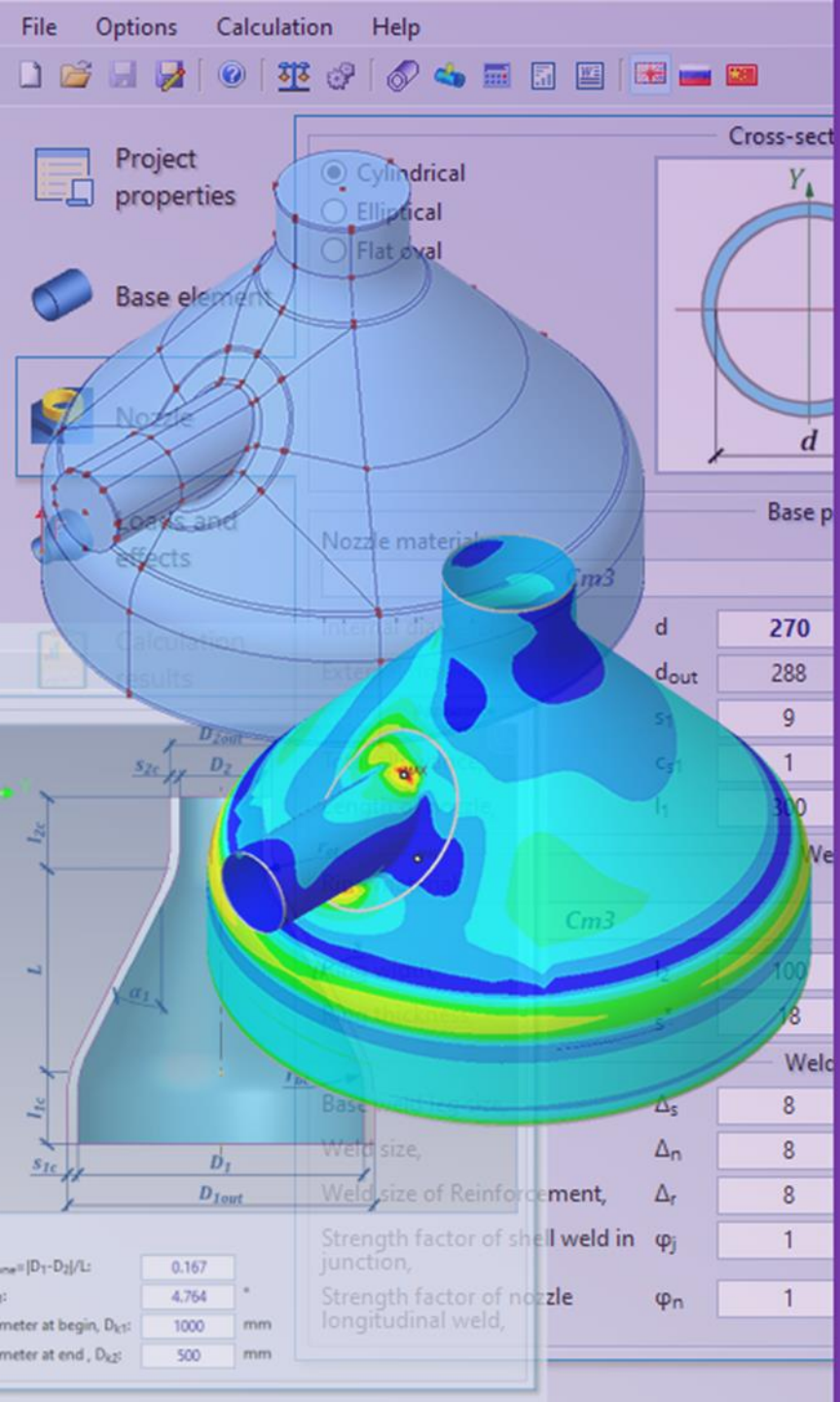
- Stresses and flexibility calculation of nozzle-shell junctions, tees, skirt support, using Finite Element Method (FEM)
- Allowable loads
- Stiffness/flexibilities of junction
- Stress Intensification Factors (SIF)
- In addition to external loads and pressure hydrostatic pressure and temperature loads can be taken into account
- Fatigue analysis (GOST 34233.3)
- Strength and stiffness calculation as per WRC537(107/297)
- Automatically generating HTML and RTF reports



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## Nozzle-FEM





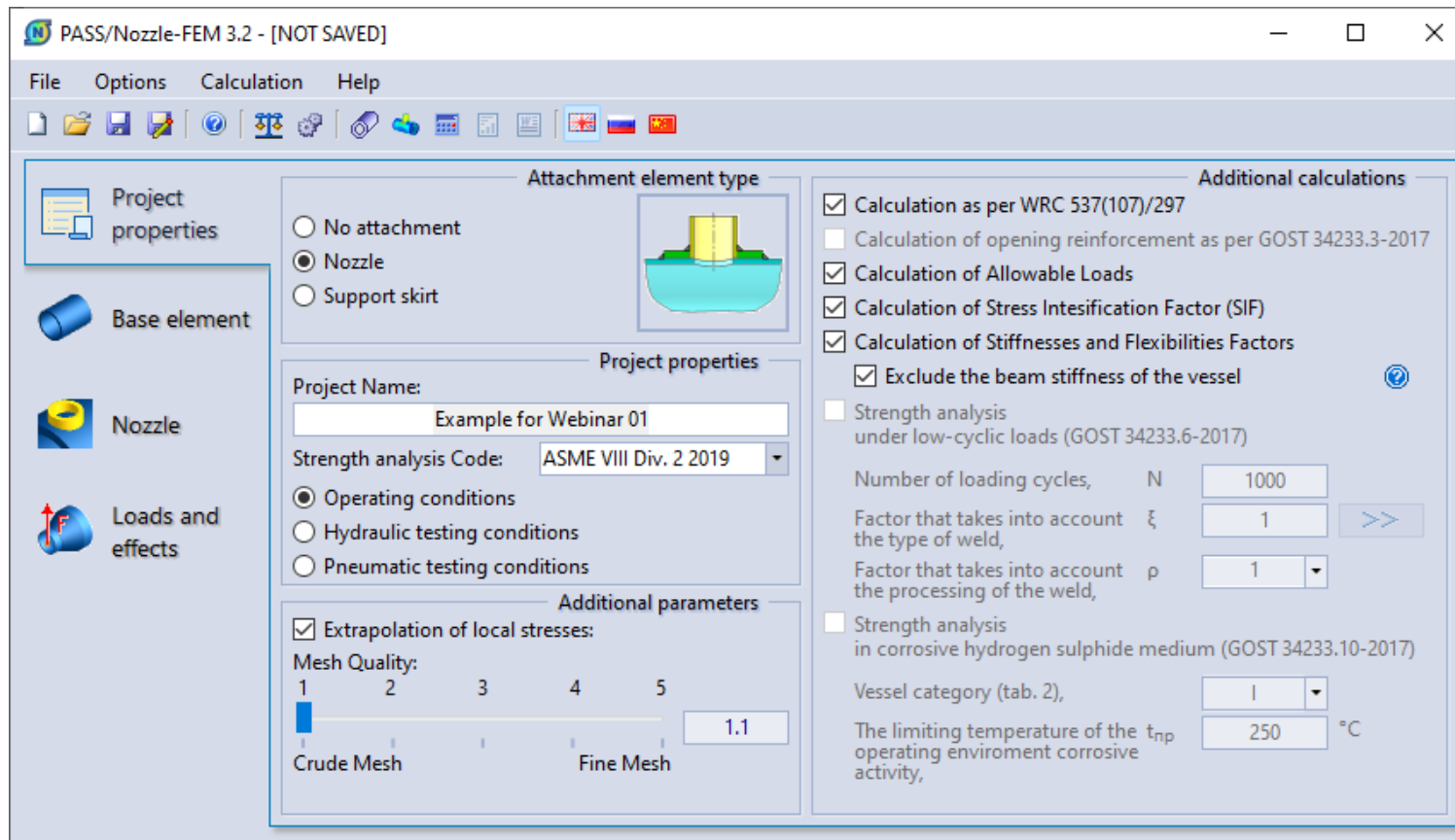
# PASS/Equip Nozzle-FEM Capabilities



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# Project properties

PASS/Equip Nozzle-FEM workspace is divided into several tabs for step-by-step setting of the input data.



# Nozzle-FEM

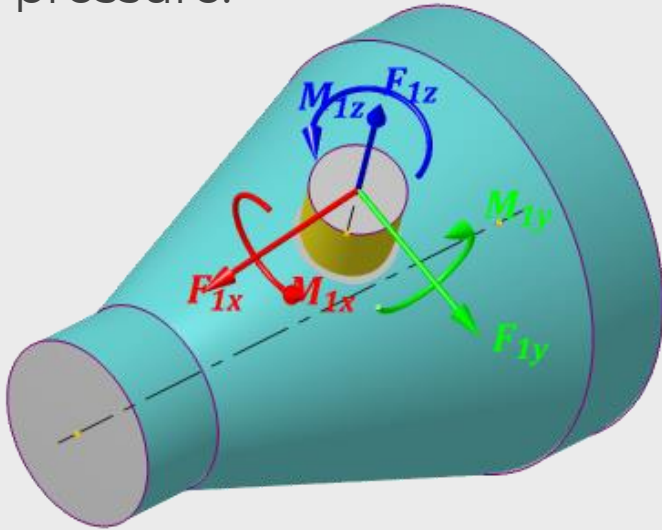
- Select an attachment element type.
- Select a code for stress analysis.
- Select additional FE-calculations (allowable loads, stiffness, SIF) and some analytical methods (like WRC).
- Set parameters to control calculation accuracy.



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# Nozzle-FEM

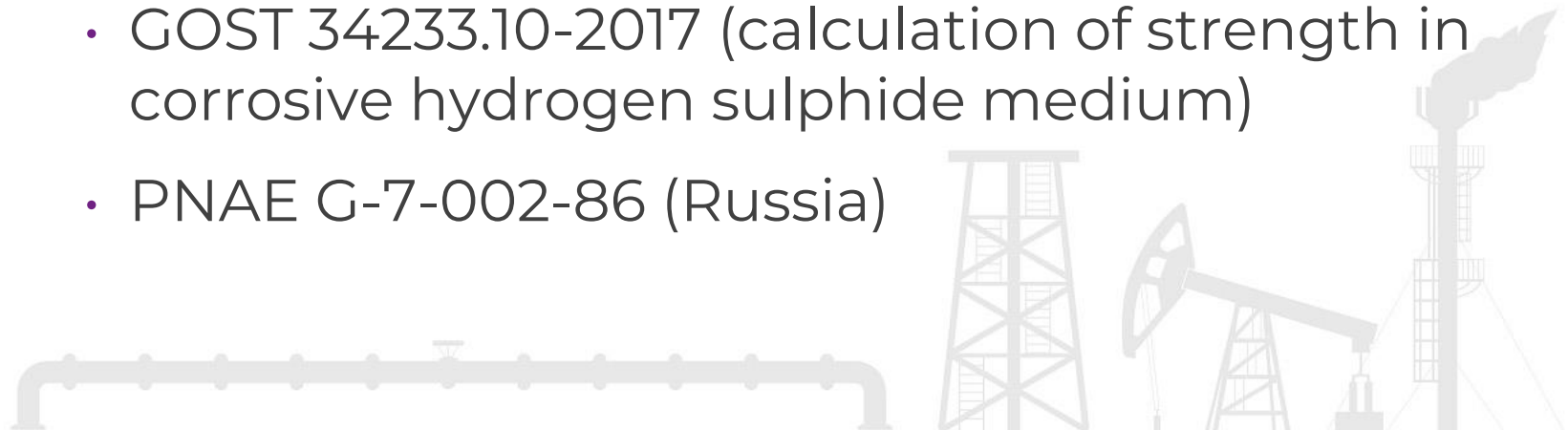
PASS/Equip Nozzle-FEM uses codes for estimating of membrane, bending, and total stresses in nozzle junction caused by external loads and pressure.



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# Supported codes

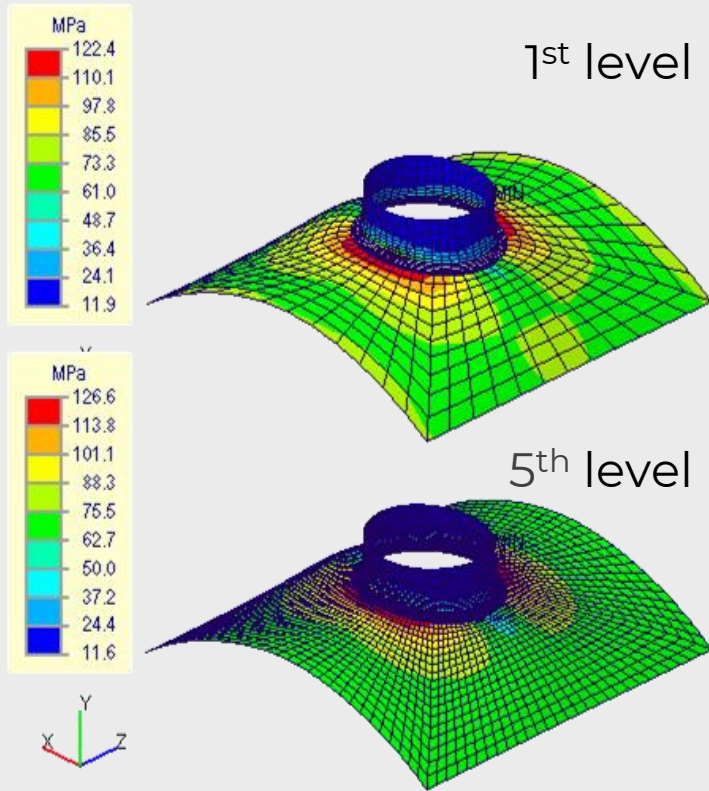
- ASME VIII–Division 1 2019 (USA)
- ASME VIII–Division 2 2019 (USA)
- EN 13445-3 2017 (European)
- JB 4732 (Chinese)
- GOST 34233.1,2,3-2017 (Russia)
- GOST 34233.6-2017 (calculation of strength under low-cyclic loads)
- GOST 34233.10-2017 (calculation of strength in corrosive hydrogen sulphide medium)
- PNAE G-7-002-86 (Russia)





# Nozzle-FEM

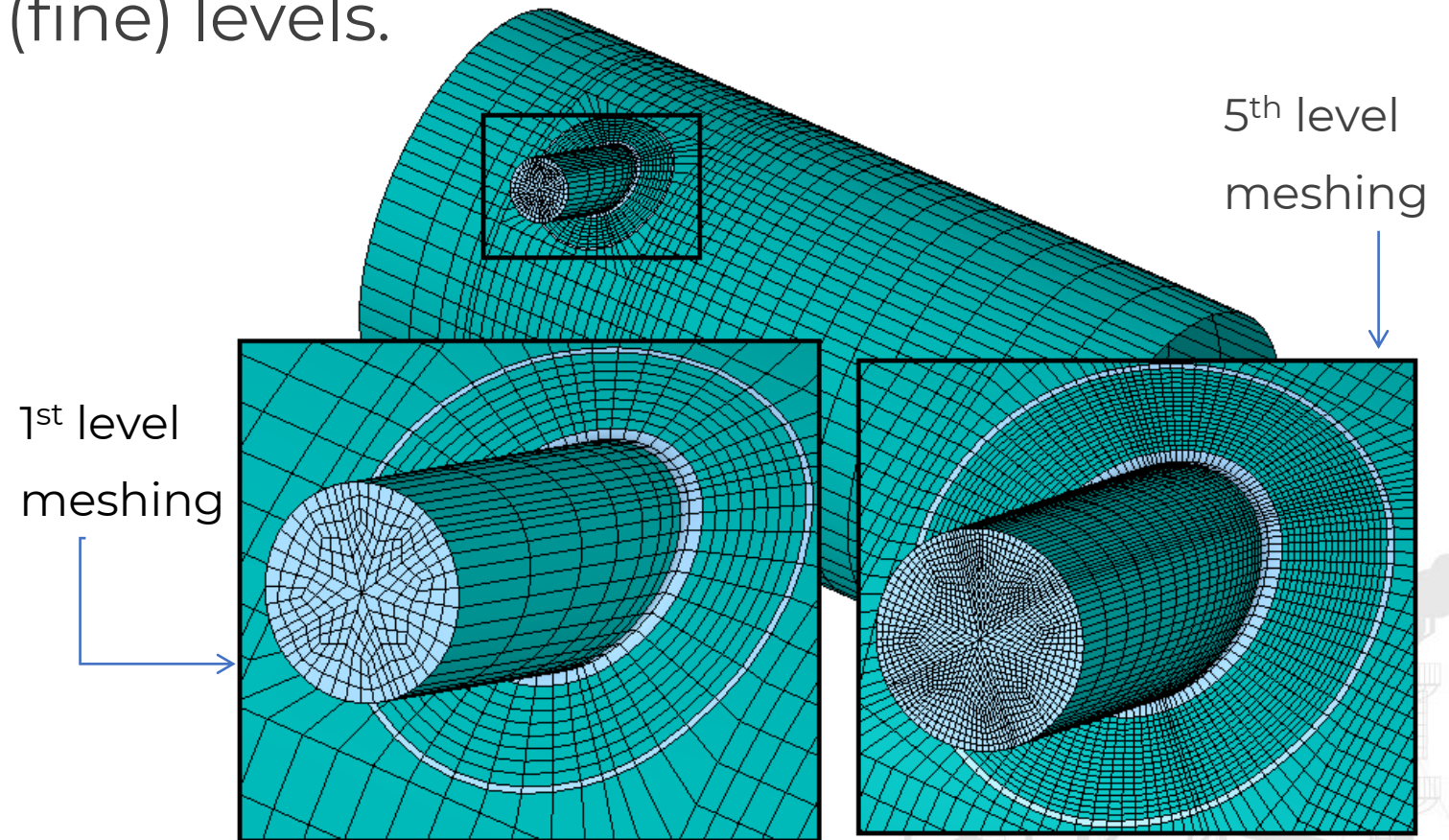
How finite element size affects the results:



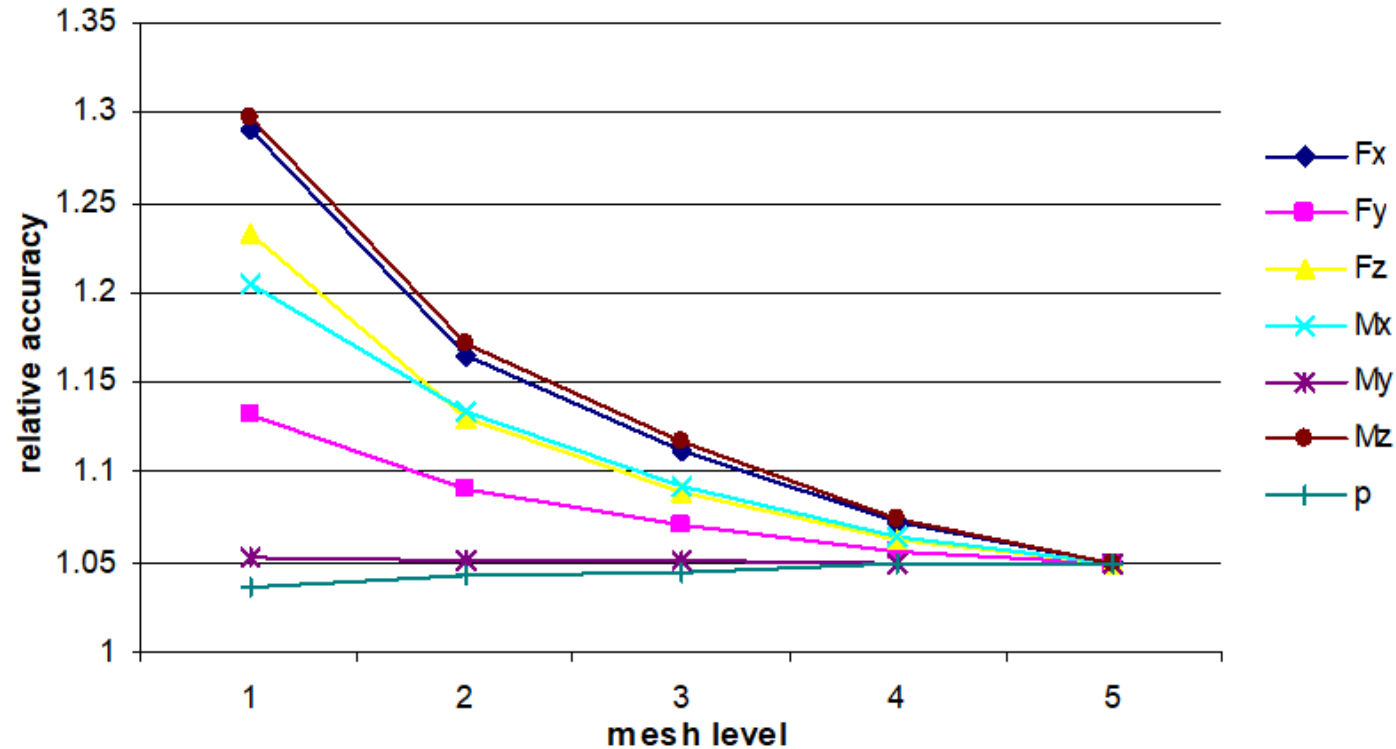
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# Accuracy of results

Results accuracy is achieved by mesh quality controlling: from 1<sup>st</sup> (crude) to 5<sup>th</sup> (fine) levels.



# Accuracy of results



Stress factor values for nozzle junction,  $K_m$

Level	1	2	3	4	5
$K_m$	1.30	1.20	1.14	1.09	1.05

## Nozzle-FEM

Lots of numerical tests allowed us:

- to define stress dependencies on mesh levels for various loads
- to define stress factor  $K_m$  used by the program in stress analysis

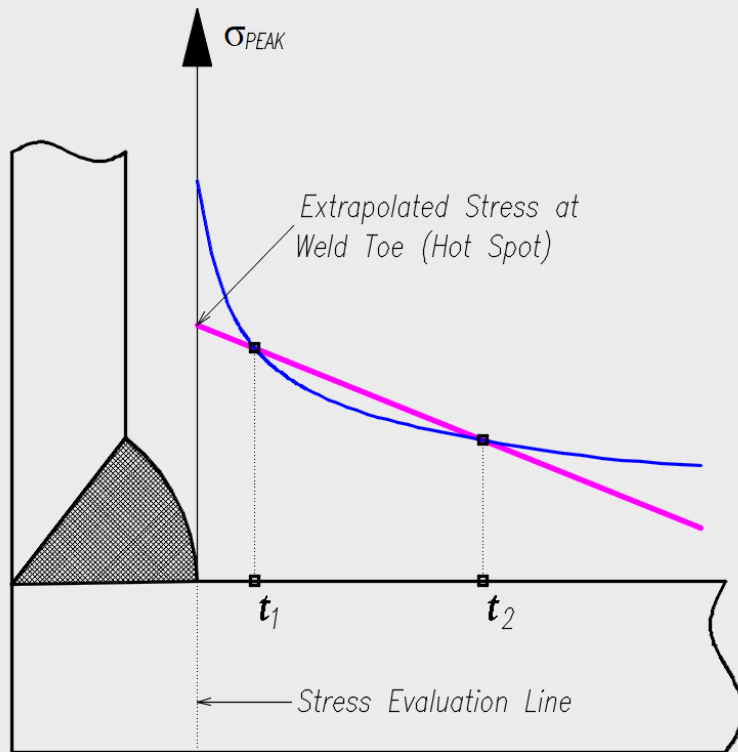


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# Nozzle-FEM

Hot Spot Stress (HSS) method [1-4]:



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# Convergence of results

To refine stress  
extrapolation  
problems:

- It allows to  
concentrate  
additional
- It increases  
refining level  
skip calculation

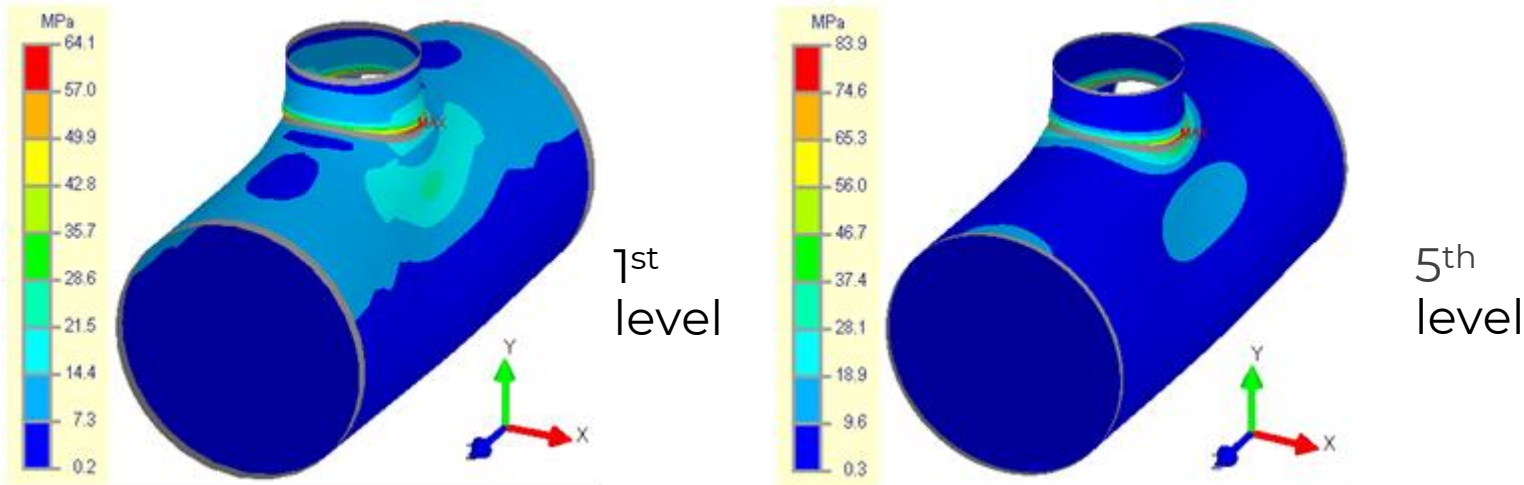
HSS uses a  
calculate stress  
at  $t_2$  by LSE de  
This approach  
around conver  
results at di

## Reference list for Hot Spot Stress method:

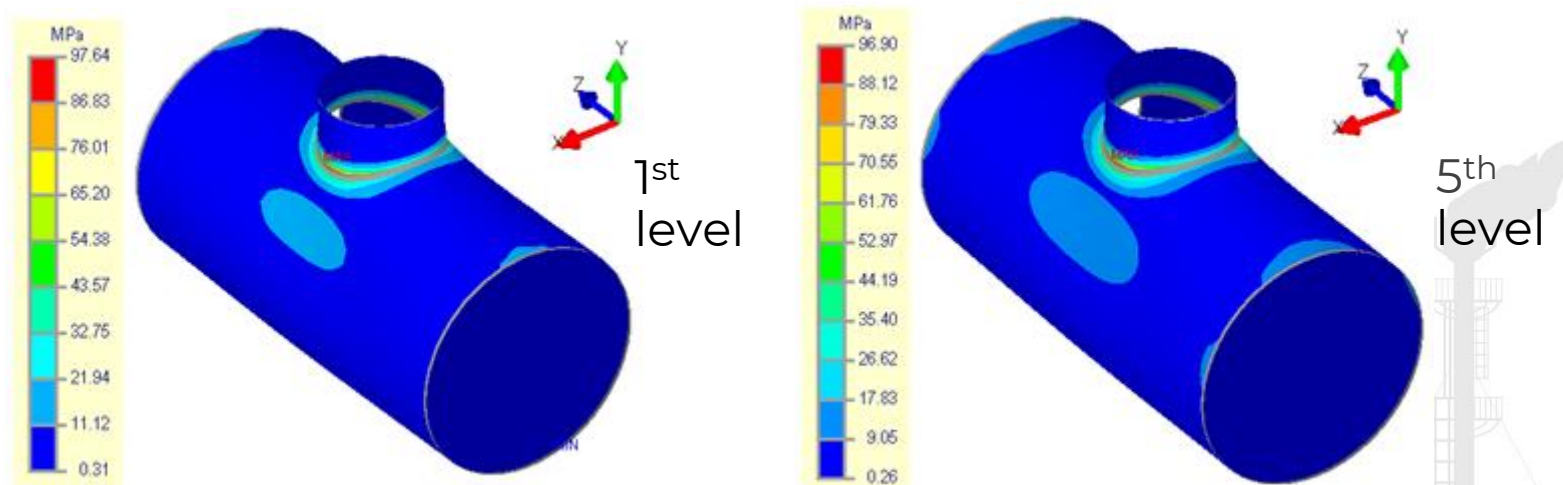
1. Fricke, W. Recommended Hot-Spot Analysis Procedure for Structural Details of Ships and FPSOs Based on Round-Robin FE Analysis [Electron. resource] / W. Fricke // Int'l J. of Offshore and Polar Engineering. – 2002. – Vol. 12, No. 1. – CD-R.
2. Maddox, C. J. Hot-Spot Stress Design Curves for Fatigue Assessment of Welded Structures [Electron. resource] / C. J. Maddox // Int'l J. of Offshore and Polar Engineering. – 2002. – Vol. 12, No 2. – CD-R.
3. Nazari, A. Application of the Hot Spot Stress Method to the Fatigue Assessment of Hollow Section Shiploader Boom Connections [Electron. resource] / A. Nazari, J. Durack // Proc. of 5th Australasian Congr. on Appl. Mechanics ACAM- 2007. – Brisbane, 2007. – CD-R.
4. Bard, W. T. Fatigue Assessment of Aluminum Ship Details by Hot-Spot Stress Approach [Text] / W. T. Bard, W. Xiaozhi, B. Stig // ABS Technical Papers, 2007. – P. 255-271.

# Convergence of results

Total stress without extrapolation stress procedure:



Total stress with **extrapolation stress** procedure:



## Nozzle-FEM

This example demonstrates that the maximum value of total stresses at 1<sup>st</sup> level did not reach the value of 5<sup>th</sup> level.

The figure below shows that the maximum peak values are not obtained even at 5<sup>th</sup> level of the mesh.

When using the stress extrapolation procedure, 1<sup>st</sup> and 5<sup>th</sup> levels of the mesh produce similar results which exceed calculation results done without applying of stresses extrapolation.



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# Nozzle-FEM

Comprehensive type set:

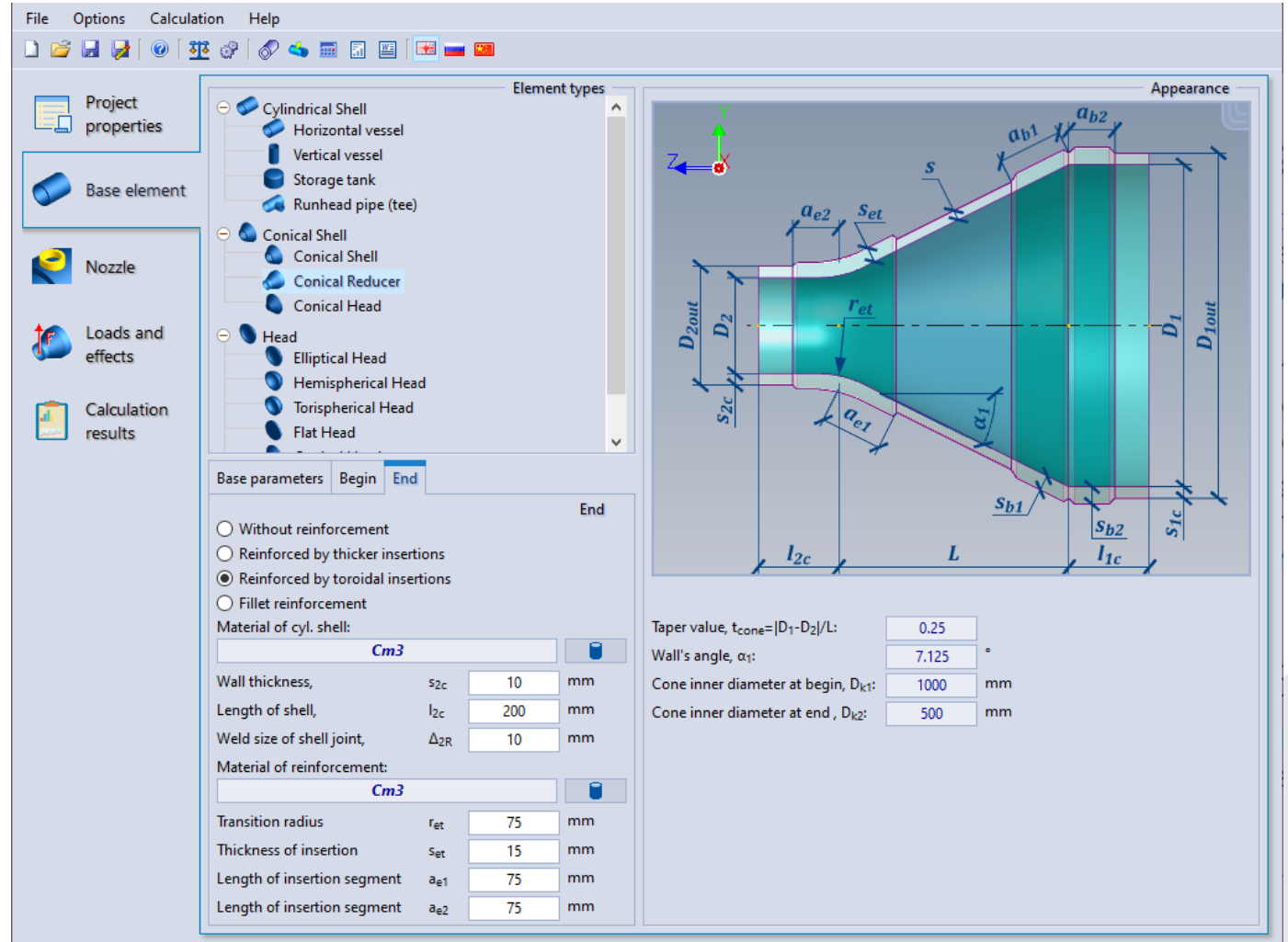
- Cylindrical shell
- Conical shell
- Storage tank (lowest course).
- Conical reducer
- Elliptical head
- Hemispherical head
- Torispherical (dished) head
- Flat head
- Cone head
- Rectangle plate (box)



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# Shell element

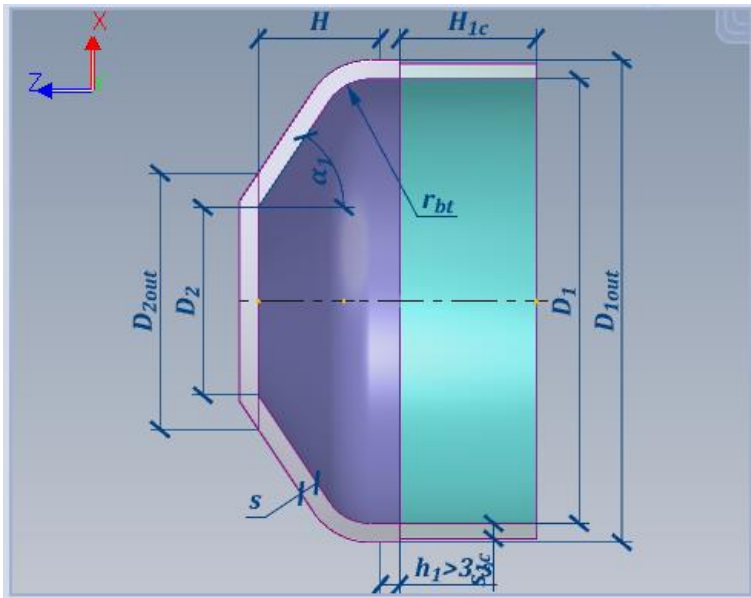
Shell tab allows to set its parameters:



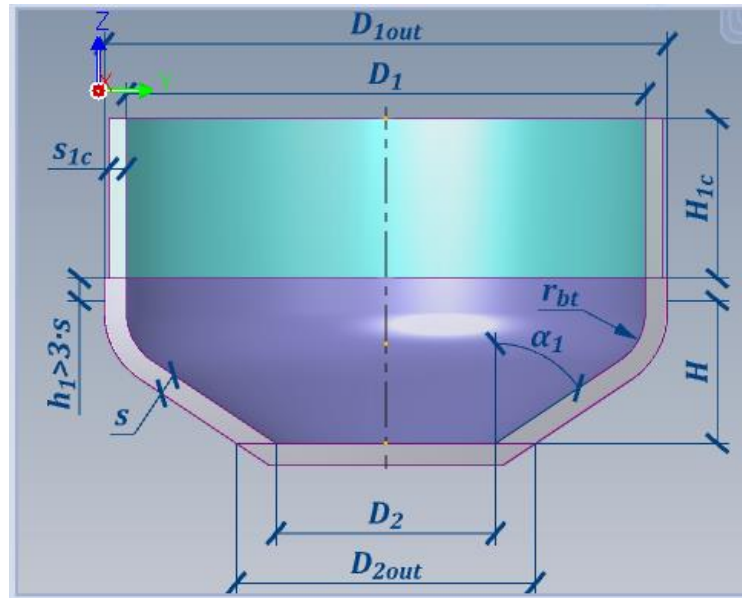
# Shell orientation features

- PASS/Equip Nozzle-FEM allows to easily change space orientation of shell
- This is important for true setting of hydrostatic pressure

Horizontal position



Invert vertical position



## Nozzle-FEM

To define space orientation, select the proper radio button:

Base parameters	
<input type="radio"/>	Horizontal placement (vertical axis X)
<input type="radio"/>	Horizontal placement (vertical axis Y)
<input checked="" type="radio"/>	Vertical placement (vertical axis Z)
<input checked="" type="checkbox"/>	Invert shell direction



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# Nozzle-FEM

Comprehensive nozzle junction set:

- With Reinforcing Pads
- With Nozzle Inserts
- With Barrel
- Trunnion connections
- Junctions in pipeline
- Storage tank nozzles (including nozzles with tombstone shape reinforcing plate)
- With beading
- With weld-in toroidal insertion



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# Nozzle tab

Nozzle tab allows to set nozzle parameters:

- Cross-section shapes
- Nozzle and reinforcement data
- Junction type
- Nozzle placement

The screenshot displays the 'Nozzle' tab interface of the PASS software. The interface is organized into several sections:

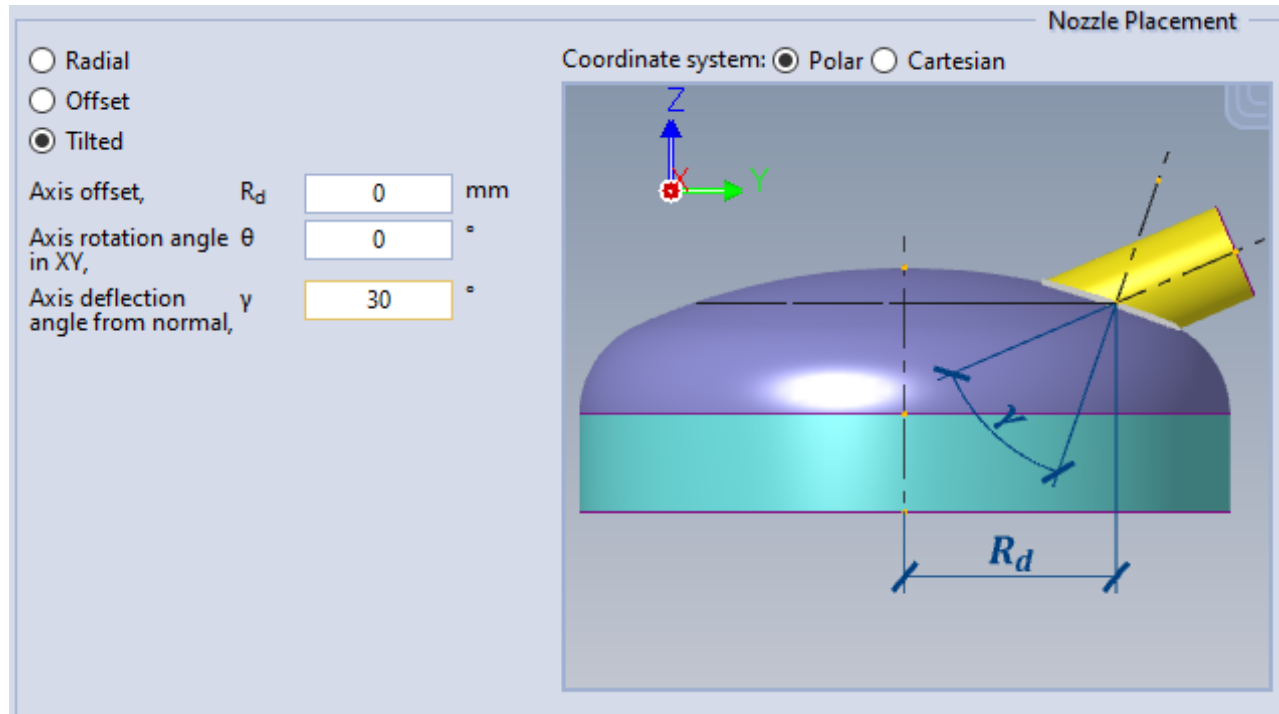
- Project properties:** Includes 'Base element' and 'Nozzle' icons.
- Types of nozzle junction:** A dropdown menu set to '2 - Passing without reinforcement'. Below it are radio buttons for 'On the edge' (checked), 'In junction' (checked), and 'Barrel' (unchecked).
- Coordinate system:** A diagram showing a 3D coordinate system with X, Y, and Z axes. The 'Coordinate system' is set to 'Polar'. Parameters include 'Z coordinate, Z<sub>0</sub>' (1000 mm), 'Axis rotation angle θ in XY' (0°), and 'Axis offset, l<sub>d</sub>' (300 mm).
- Base parameters:** A table for defining nozzle dimensions:

Nozzle material:	
Internal diameter, d	500 mm
External diameter, d <sub>out</sub>	520 mm
Wall thickness, s <sub>1</sub>	10 mm
Total allowance, c <sub>s1</sub>	0 mm
Length of nozzle, l <sub>1</sub>	200 mm
Internal part length, l <sub>3</sub>	0 mm
Corrosion allowance, c <sub>s3</sub>	0 mm
- Welded Seams:** A table for defining weld parameters:

Base weld leg size, Δ <sub>s</sub>	10 mm
Weld size, Δ <sub>n</sub>	10 mm
Weld size on nozzle internal part, Δ <sub>ni</sub>	8 mm
Strength factor of shell weld in junction, φ <sub>j</sub>	1
Strength factor of nozzle longitudinal weld, φ <sub>n</sub>	1

# Nozzle placement features

- There is a big set of nozzle orientation ways
- Different view is provided for each dimension field



# Nozzle-FEM

Comprehensive orientation set:

- Radial
- Hillside Offset
- Tilted
- Polar and Cartesian coordinates placement
- Tilted in section plane
- Vector



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# Nozzle-FEM

Key features:

- Load cases adding
- Concentrated loads (in global, local and pipe CS)
- Thermal strains
- Inner/outer pressure
- Hydrostatic pressure

Loads can be automatically converted when switching between different coordinate systems.



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# Loads and effects

**Project properties**

**Base element**

**Nozzle**

**Loads and effects**

**Calculation results**

**Load cases**

Loadcase : (1)

Append Delete Clear All

**Design pressure**

☒ Internal ☐ External p 0 MPa

☐ Add hydrostatic pressure

Height of filling H 2000 mm

Density of medium  $\rho$  1000 kg/m<sup>3</sup>

**Temperature effect**

☐ Add thermal strains

Design temperature of shell T 150 °C

Design temperature of nozzle T<sub>n</sub> 20 °C

Reference temperature T<sub>0</sub> 20 °C

**Base element**

Coordinate system:

☒ Shell ☒ Pipe

**Load values:**

F <sub>2x</sub>	0	tf
F <sub>2y</sub>	0	tf
F <sub>2z</sub>	203.94	tf
M <sub>2x</sub>	0	tf·m
M <sub>2y</sub>	0	tf·m
M <sub>2z</sub>	0	tf·m

**Nozzle**

Coordinate system:

☐ Shell ☒ Nozzle ☒ Pipe

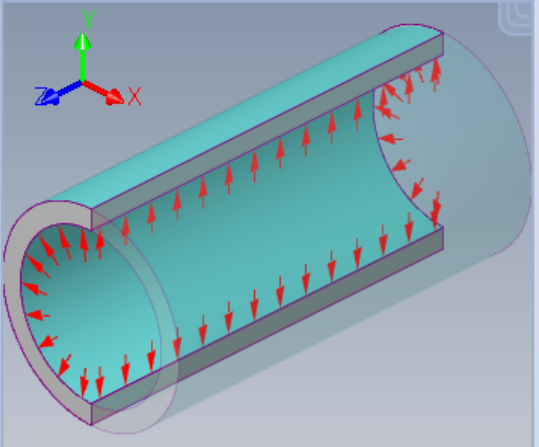
Load place:

☒ On the edge ☒ In junction

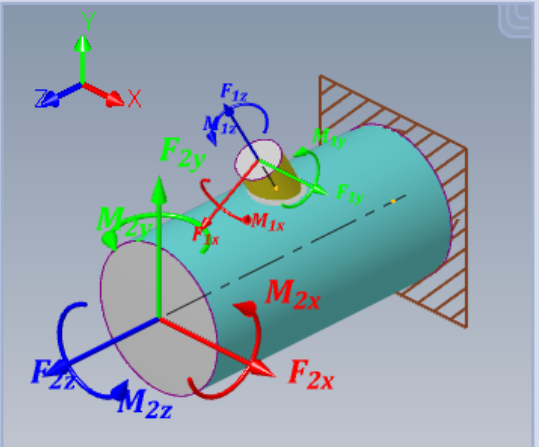
**Load values:**

F <sub>1x</sub>	0	tf
F <sub>1y</sub>	0	tf
F <sub>1z</sub>	10.2	tf
M <sub>1x</sub>	0	tf·m
M <sub>1y</sub>	0	tf·m
M <sub>1z</sub>	0	tf·m

**Effects**



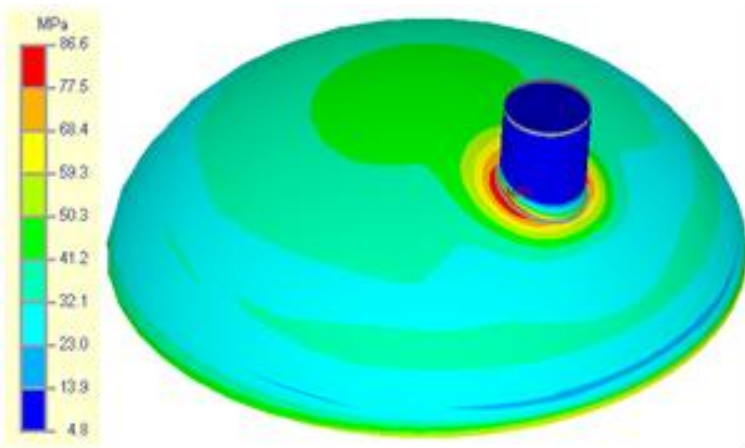
**Concentrated loads**



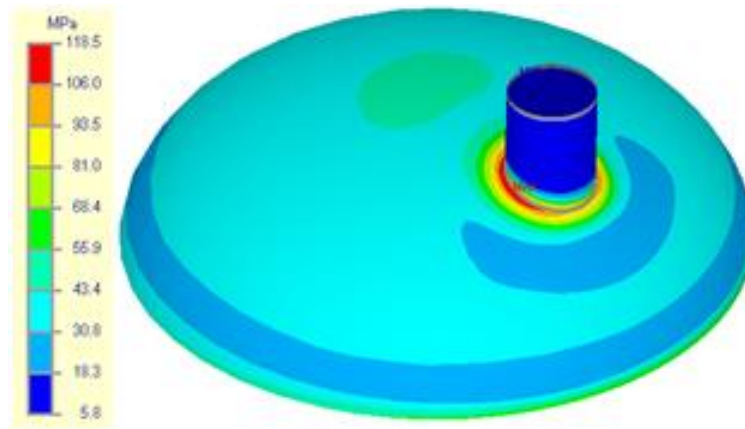
# Thermal strains

PASS/Equip Nozzle-FEM considers thermal expansion (deformation) of structure element materials that causes additional stresses by constrained deformations (different linear expansion coefficients, temperatures, etc.)

Without thermal strains



With thermal strains



## Nozzle-FEM

Difference between shell and nozzle material thermal expansion factors leads to a constrained thermal deformation and additional stresses.

Stresses can drastically increase in the nozzle junction area.

In the example, it increases by 32MPa (37%).

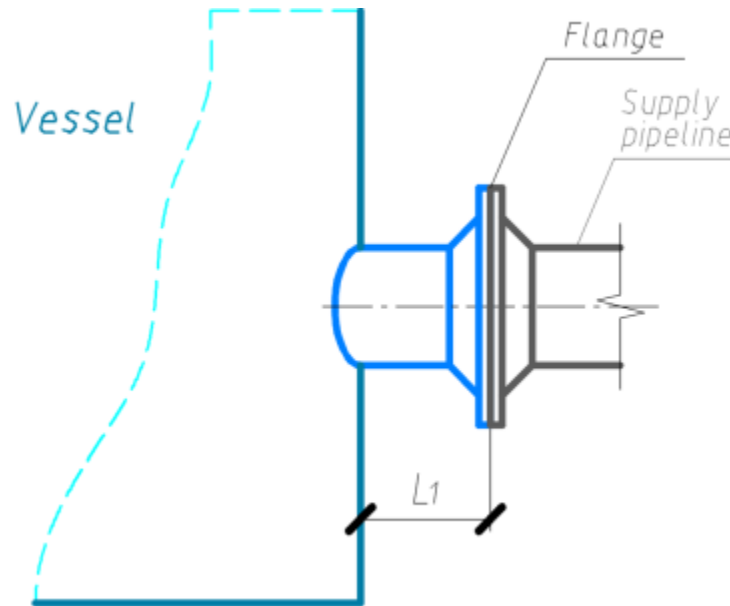


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# Loads setting

Nozzle-FEM provides two ways to set loads on nozzle: «On the edge» and «In junction», that are different in definition of nozzle length.

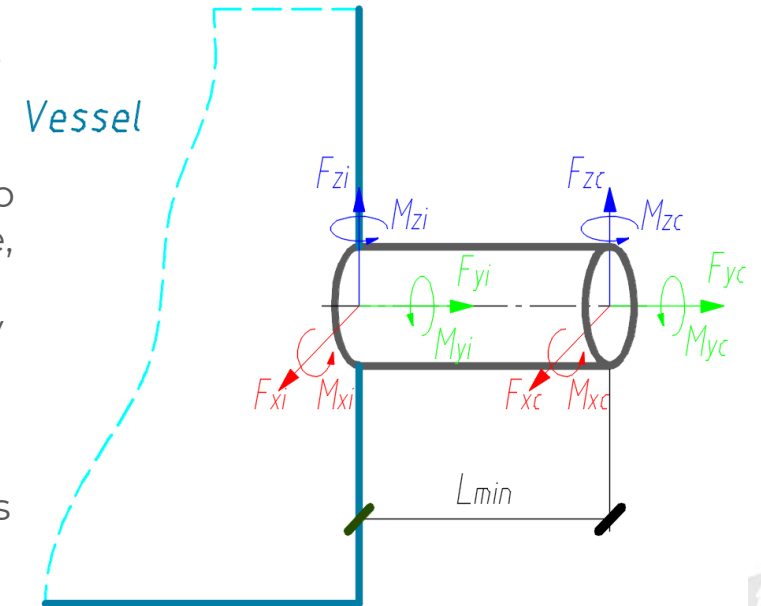
**On the edge** – a typical case when the nozzle and supply pipelines are connected by flange. In this case, the design scheme, including the supply pipelines, ends on a flange connection, and the design loads on the nozzle are obtained at this point.



Nozzle length is calculated as:

$$L_1 \geq \max\{\delta, \delta_2, r\} + \min\{s, s_1\}.$$

**In junction** – a case when the supply pipeline ends at the place of junction into the shell. In this case, the design scheme, including the supply pipelines, usually ends on the outer surface of the shell, and the design loads on the nozzle are obtained at this point.



Nozzle length is calculated as [see ASME B31J-2017]:

$$L_{min} = \min\{0.5d_{cp}^{1.4} s_1^{-0.4}, d\}.$$

# Nozzle-FEM

Calculation “in Junction” corresponds to the “flexible” connection between the pipeline and the shell, and has been obtained based on numerous field tests [ASME B31J-2017].

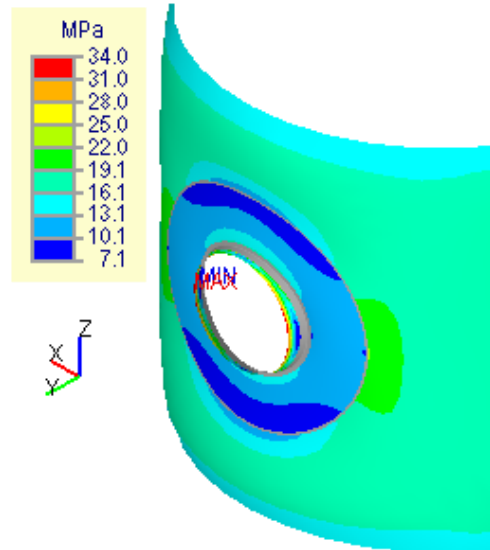
It allows engineers to consider an ovalization of the section at the junction area that corresponds to the “flexible” connection between the pipeline and the shell.



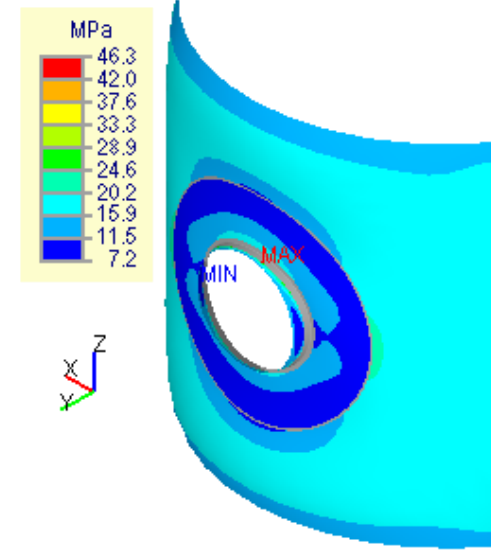
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## Loads setting in junction

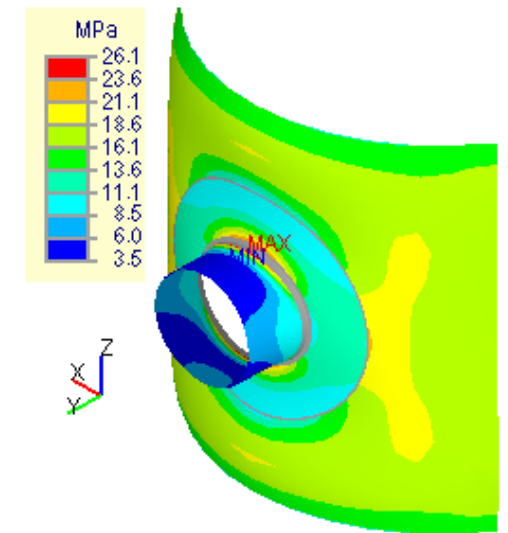
The influence of edge effect on results in junction:



L=30mm – well-defined edge effect from the load application



L=50mm – short length of the nozzle, falls within the area of the edge effect of the load application



At the nozzle length obtained by formula

$$L_{min} = \min\{0.5d_{cp}^{1.4} s_1^{-0.4}, d\}.$$



# Nozzle-FEM

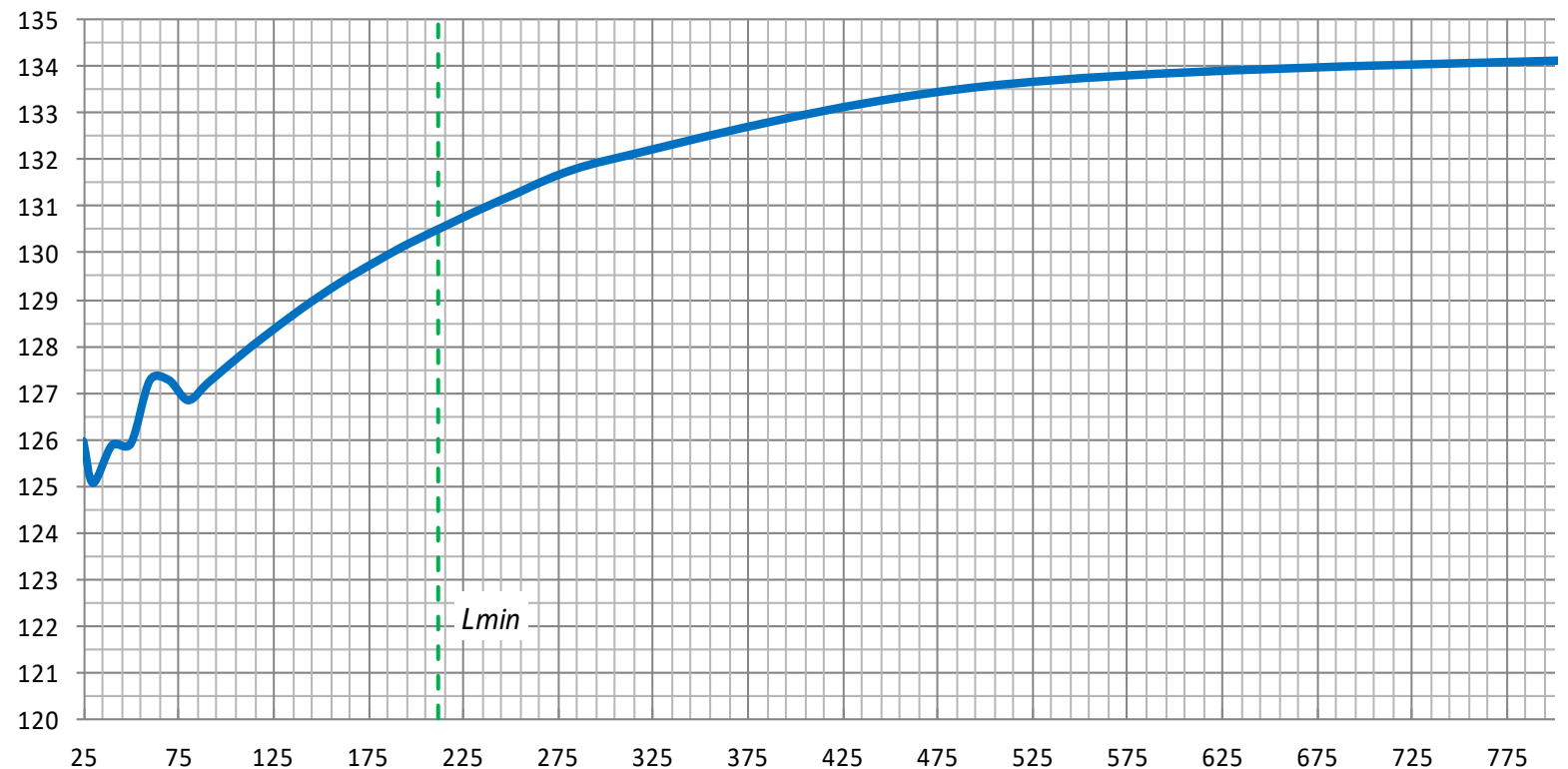
When calculating the strength, PASS/Equip Nozzle-FEM software automatically converts the loads specified by the user at the junction point into statically equivalent loads



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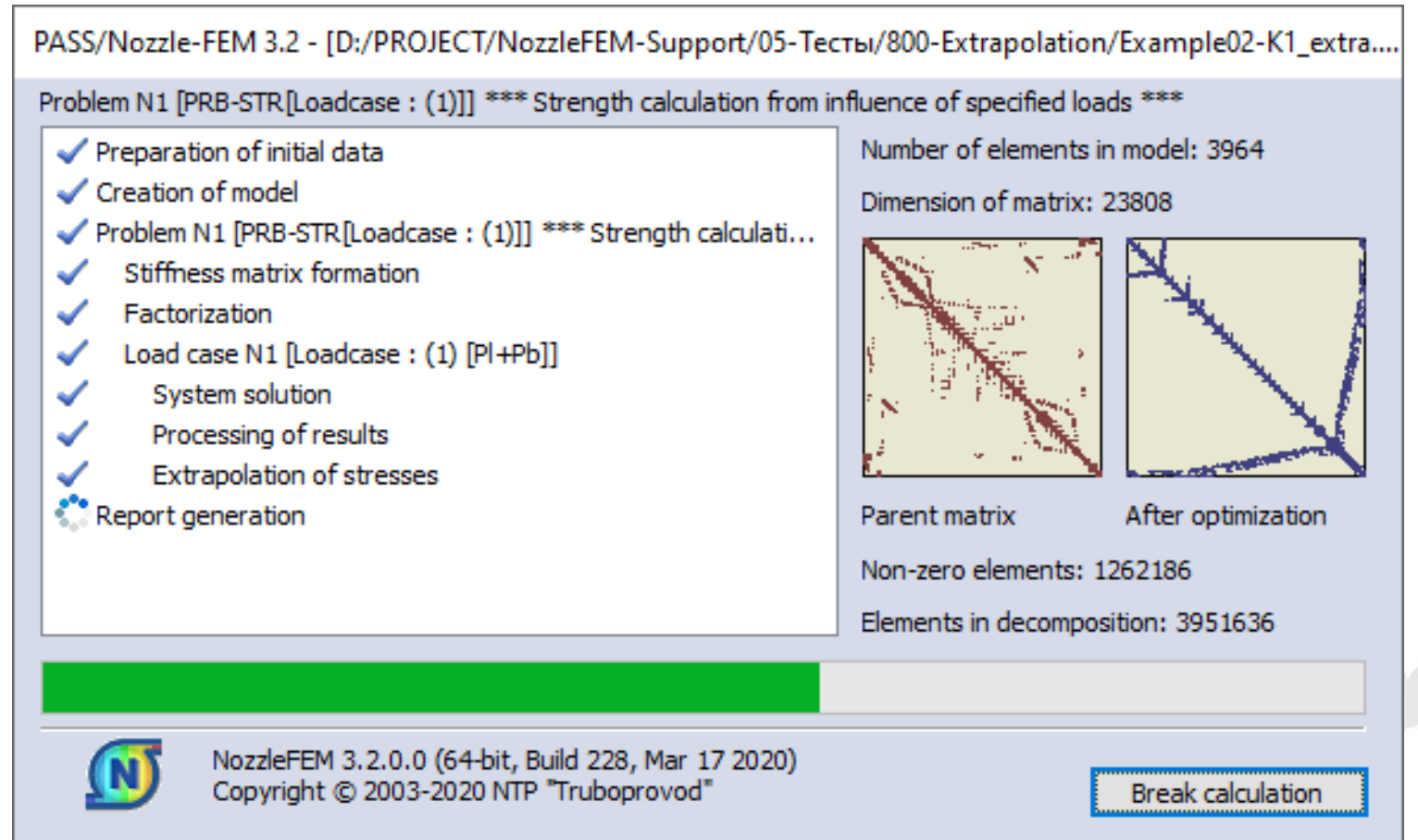
# Loads setting in junction

The plot represents the change curve in the allowable axial force depending on the nozzle length, which shows that, in the junction area, at a distance less than 100 mm, edge effects from the load application point appear ( $D=2000\text{mm}$ ,  $s=12\text{mm}$ ,  $d=203$ ,  $s_1=6\text{ mm}$ ).



## Calculation stage

- Checking data Input
- Creation of models (geometric, finite-element)
- Solution
- Results/stress analysis
- Html report generation





# Nozzle-FEM

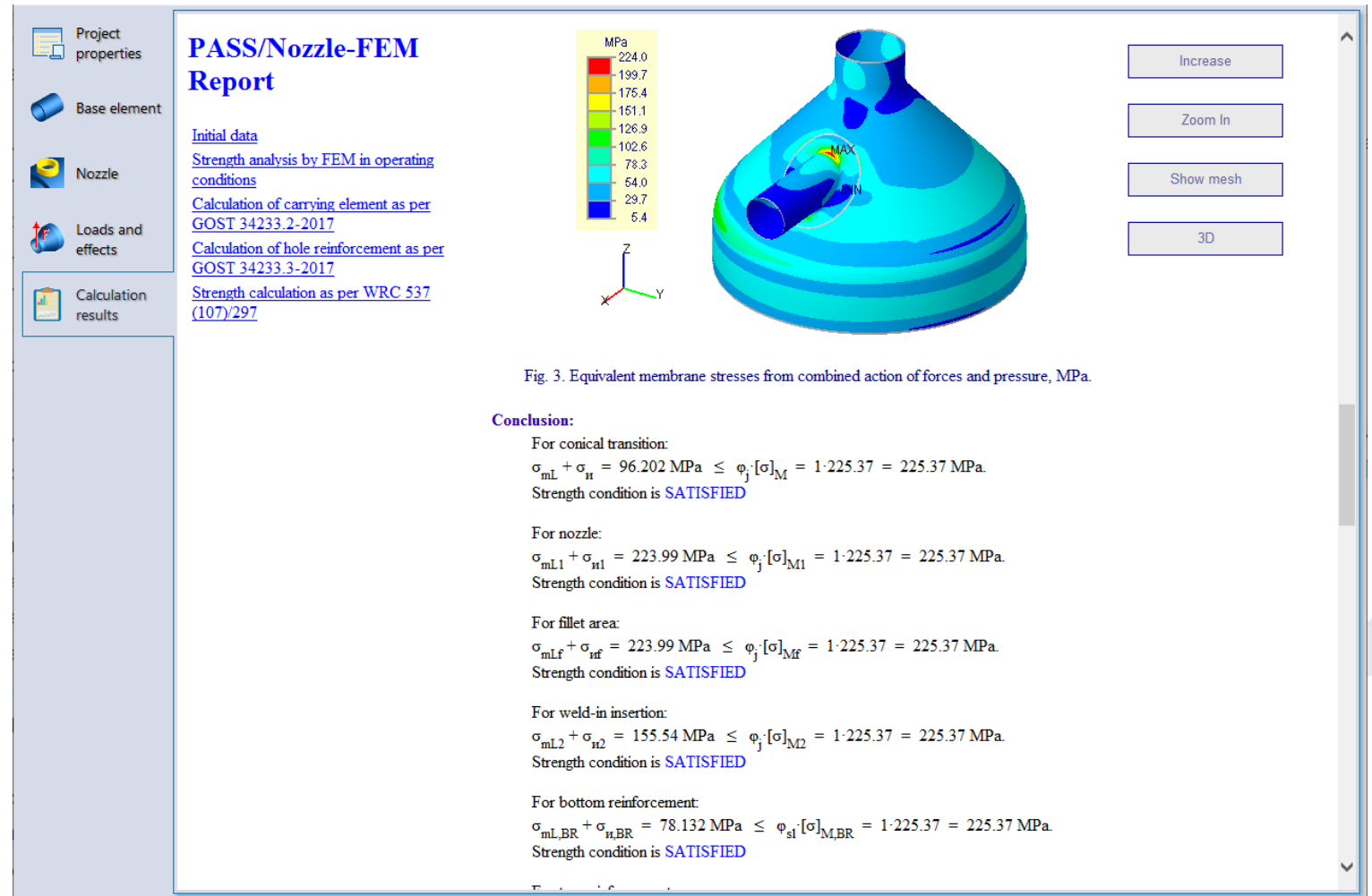
- General report is provided in HTML.
- It contains input data, strength analysis, etc.
- RTF format can be generated.
- 3D-postprocessor from the report.



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# Comprehensive report content

## Intuitive report



# Report with allowable loads

Allowable loads on nozzle junction are presented:

File Options Calculation Help

Project properties  
Base element  
Nozzle  
Loads and effects  
Calculation results

## PASS/Nozzle-FEM Report

[Initial data](#)  
[Strength analysis by FEM in operating conditions](#)  
[Allowable loads](#)  
[Stiffness and flexibilities](#)  
[Stress intensification factors](#)  
[Calculation of carrying element as per GOST 34233.2-2017](#)  
[Calculation of hole reinforcement as per GOST 34233.3-2017](#)  
[Strength calculation as per WRC 537\(107\)/297](#)

### Allowable loads

Allowable individual loads without influence of other loads, including pressure<sup>1</sup>

Location	Allowable forces, kN			Allowable moments, kN·m			Allowable pressure, MPa
	F <sub>x</sub>	F <sub>y</sub>	F <sub>z</sub>	M <sub>x</sub>	M <sub>y</sub>	M <sub>z</sub>	[p]
runhead pipe (global CS)	520.572	1015.22	2384.95	609.704	1652.08	512.642	1.16
elbow part end (local CS)	47.978	21.09	71.804	4.16			

Note:  
1. When exceeding any loading component, a reinforcing of nozzle connect

Press to pass values to PASS/Start-Prof

### Allowable loads at the design pressure<sup>2</sup>

Under action of temperature strains allowable loads is multiplied by additional factor  $n_{temp}$  for loadcase with only temperature strains:  
 $f_{temp} = \max\{1 - 1/n_{temp}; 0.0\} = \max\{1 - 1/\infty; 0.0\} = 1.$

Under action of design pressure allowable loads is multiplied by additional factor:  
 $f_{press} = \max\{1 - \alpha_p p/[p]; 0.0\} = \max\{1 - 1/1.46; 0.0\} = 0.316,$   
 $f_{press} = \max\{1 - \alpha_p p/[p]; 0.0\} = \max\{1 - 1/1.45; 0.0\} = 0.312,$   
where  $\alpha_p$  - factor equal to 0.87 for PNAE-G-7-002-86, and in other cases it is assumed to be 1.0.

Location	Allowable forces, kN			Allowable moments, kN·m			Design pressure, MPa
	F <sub>x</sub>	F <sub>y</sub>	F <sub>z</sub>	M <sub>x</sub>	M <sub>y</sub>	M <sub>z</sub>	p
runhead pipe (global CS)	54.884	107.03	251.44	64.281	174.28	54.153	1
elbow part end (local CS)	4.987	2.19	7.464	0.432	1.11	4.033	1

Note:  
2. When exceeding one or several loading components, a supplementary strength analysis is required

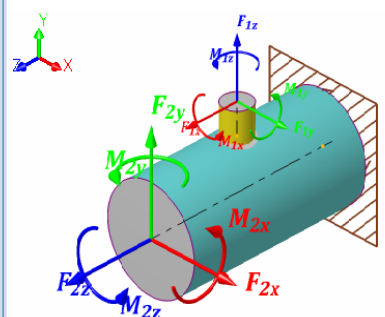


Fig. 6. The coordinate systems of runhead pipe and elbow part.

# Nozzle-FEM

- 1<sup>st</sup> table: for individual allowable loads without influence of other loads
- 2<sup>st</sup> table: for allowable loads that take into account their combined action



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# Nozzle-FEM

If option “Exclude beam stiffness” is enabled, then it additionally displays a table of flexibilities factors for programs like PASS/Start-Prof.

Table of flexibility factors

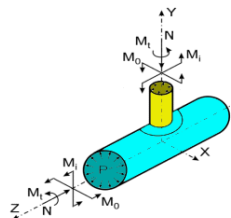


Fig. 8. The coordinate system for determining the flexibility factors.

Description		Main part	Branch part
From axial force N	$k_a$	0.012	5.919
From inplane bending moment $M_i$	$k_i$	0.036	7.352
From outplane bending moment $M_o$	$k_o$	$9.493 \cdot 10^{-12}$	19.11
From torsion moment $M_t$	$k_t$	0.034	0.221

# Report with stiffness/flexibilities

Project properties

Base element

Nozzle

Loads and effects

Calculation results

### PASS/Nozzle-FEM Report

[Initial data](#)  
[Strength analysis by FEM in operating conditions](#)  
[Allowable loads](#)  
[Stiffness and flexibilities](#)  
[Stress intensification factors](#)  
[Calculation of carrying element as per GOST 34233.2-2017](#)  
[Calculation of hole reinforcement as per GOST 34233.3-2017](#)  
[Strength calculation as per WRC 537\(107\)/297](#)

### Stiffness and flexibilities

The nozzle junction stiffnesses and flexibilities was calculated with parent shell fixed at both ends.

Fig. 7. The coordinate systems of runhead pipe and elbow part.

#### The stiffness table

The calculated stiffness values are shown in the table below:

Location	Linear, kN/m			Angular, kN·m/deg		
	KL <sub>x</sub>	KL <sub>y</sub>	KL <sub>z</sub>	KR <sub>x</sub>	KR <sub>y</sub>	KR <sub>z</sub>
runhead pipe (global CS)	$3.286 \cdot 10^7$	$2.633 \cdot 10^8$	$6.413 \cdot 10^8$	$4.574 \cdot 10^5$	$1.745 \cdot 10^{15}$	$3.772 \cdot 10^5$
elbow part end (local CS)	$7.674 \cdot 10^4$	$3.924 \cdot 10^4$	$1.758 \cdot 10^5$	23.83	61.92	1586.86

#### The flexibilities table

The calculated flexibilities values are shown in the table below:

Location	Linear, (kN/m) <sup>-1</sup>			Angular, (kN·m/deg) <sup>-1</sup>		
	FL <sub>x</sub>	FL <sub>y</sub>	FL <sub>z</sub>	FR <sub>x</sub>	FR <sub>y</sub>	FR <sub>z</sub>
runhead pipe (global CS)	$3.043 \cdot 10^{-8}$	$3.798 \cdot 10^{-9}$	$1.559 \cdot 10^{-9}$	$2.186 \cdot 10^{-6}$	$5.730 \cdot 10^{-16}$	$2.651 \cdot 10^{-6}$
elbow part end (local CS)	$1.303 \cdot 10^{-5}$	$2.549 \cdot 10^{-5}$	$5.690 \cdot 10^{-6}$	0.042	0.016	$6.302 \cdot 10^{-4}$

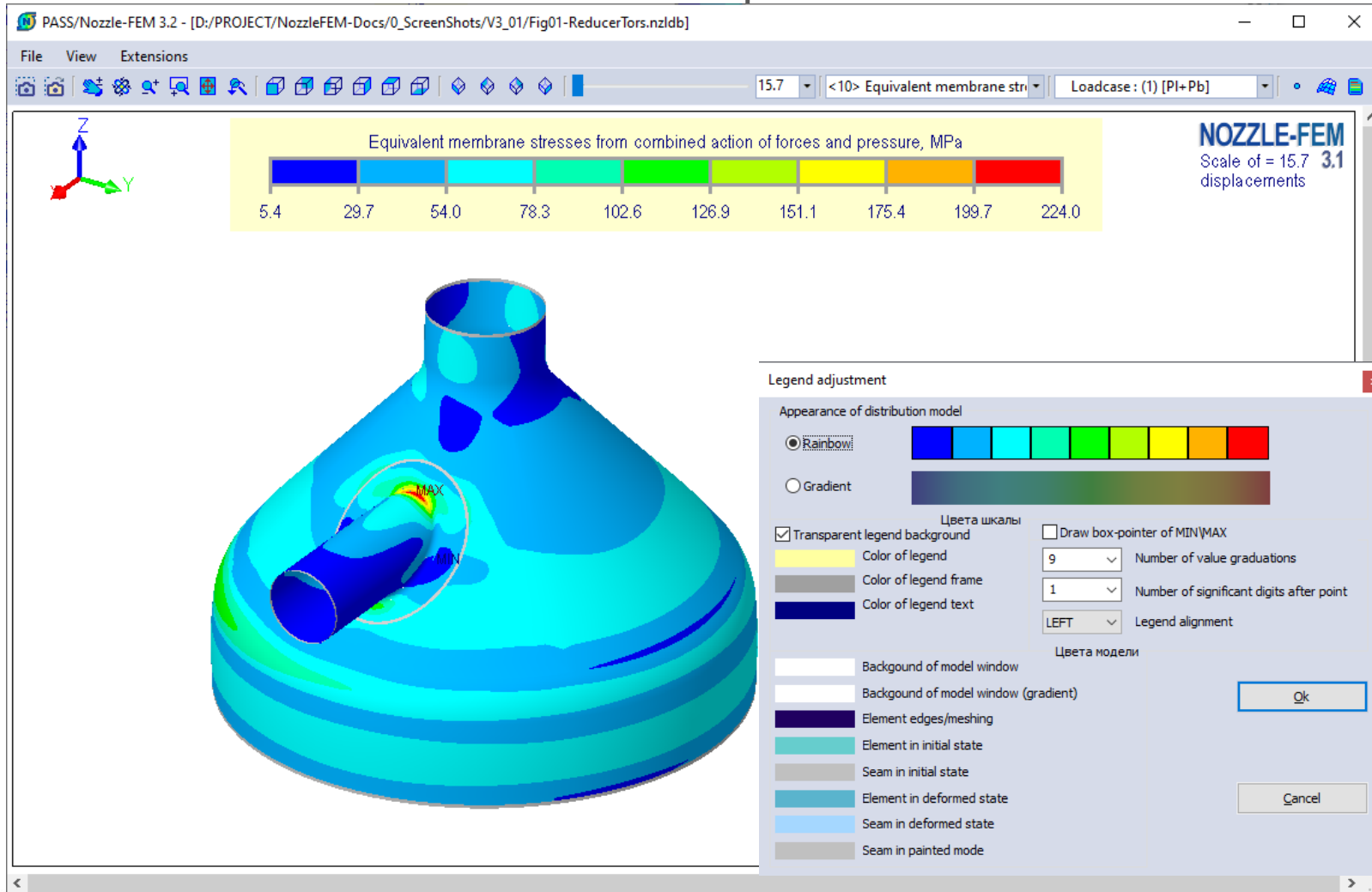
Press to pass values to PASS/Start-Prof

Copy

Copy

# 3D processor features

## Launched from Html report



# Nozzle-FEM

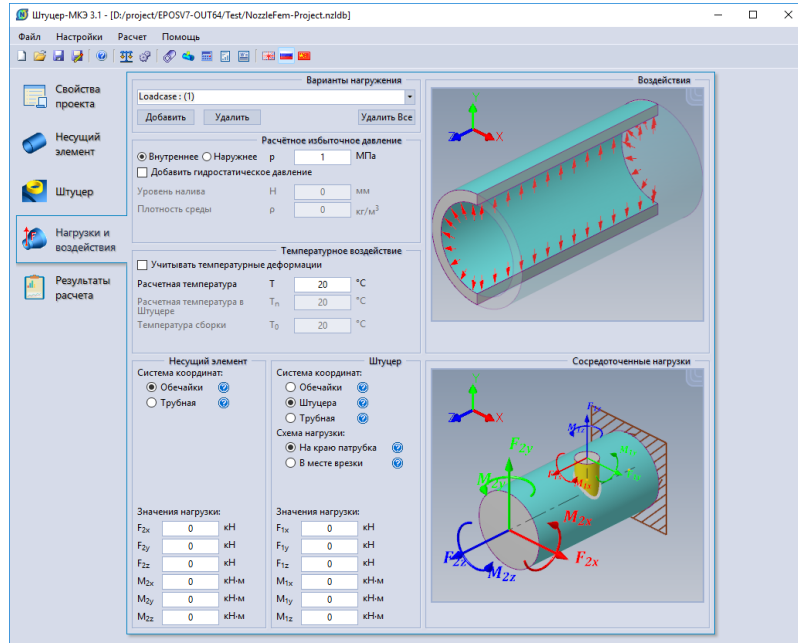
## Capabilities:

- Change view
- Make screenshots
- Choose different paint modes
- Change load case
- Change color set
- Etc.

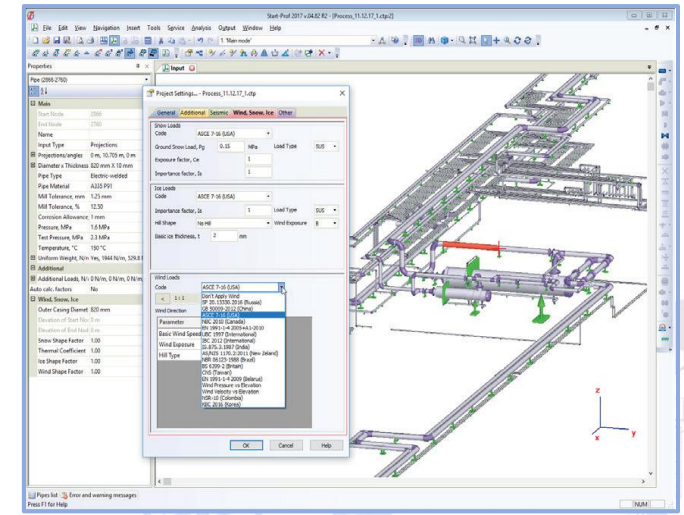
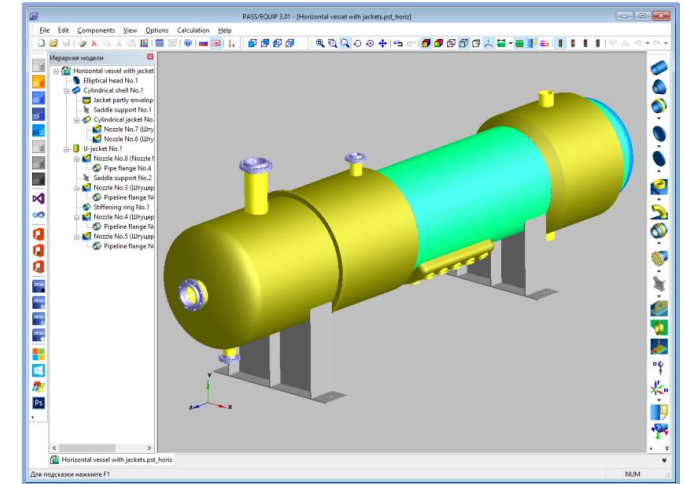
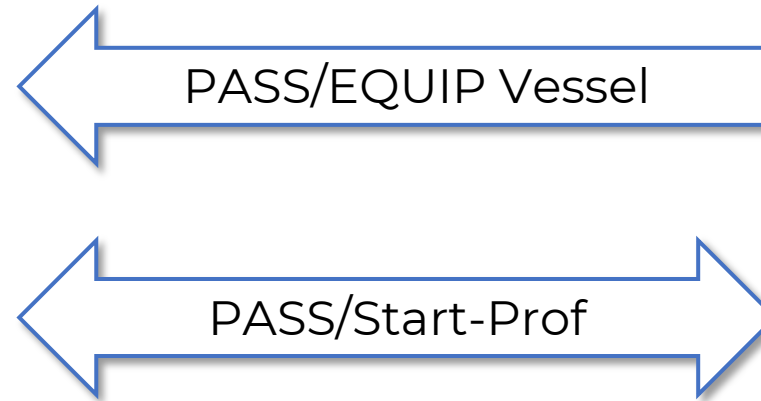


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## Integration capabilities

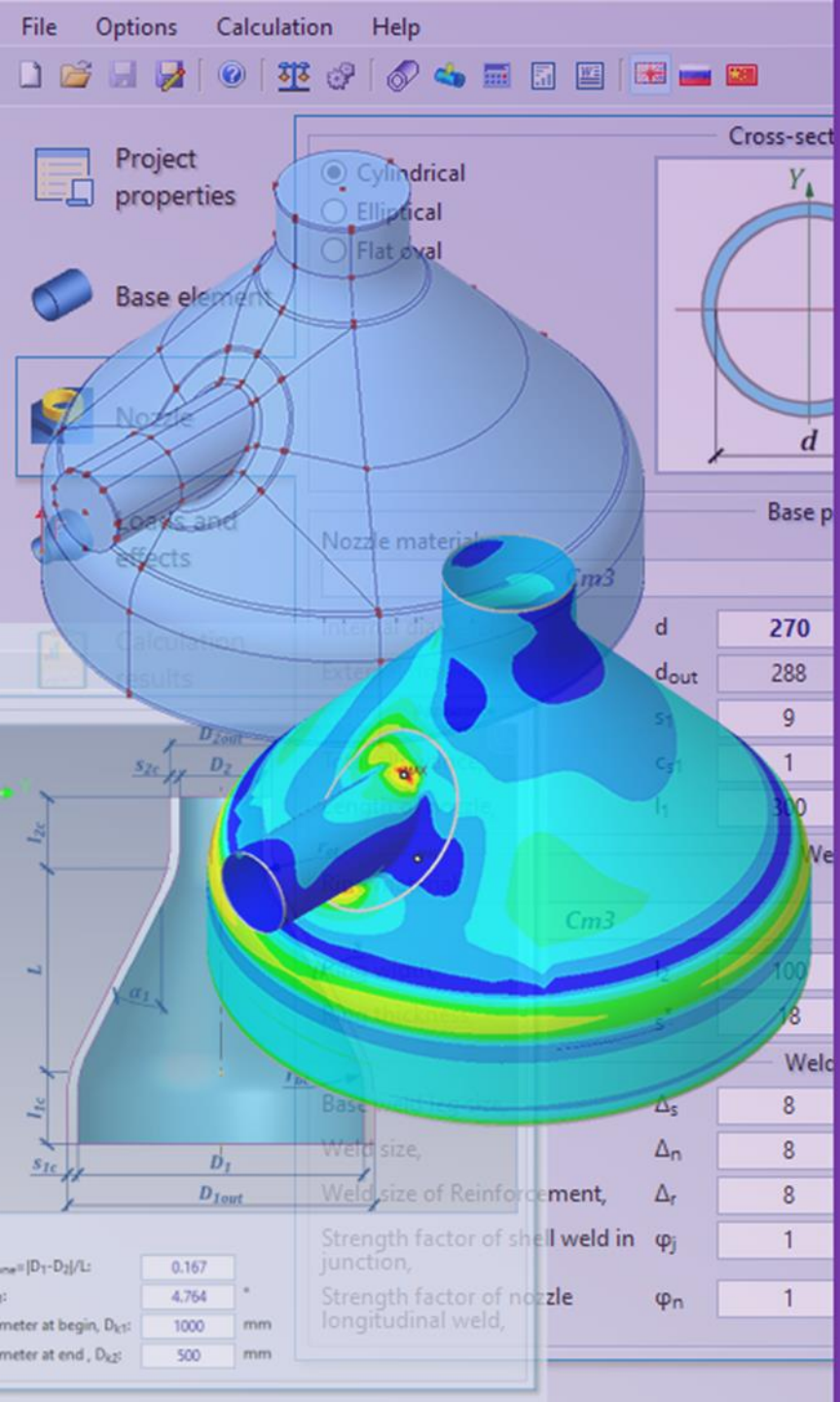


- PASS/EQUIP vessel allows to pass and to export (nzi-files) any part of model



- Export calculated values from report to PASS/Start-Prof
- Calculation module as per WRC107(537)/297 and GOST 34233.3
- **Future plans of full integration:** Start-Prof will run Nozzle-FEM for numerical calculation (FEM) of nozzle junctions, nozzle-to-shell stiffness/flexibilities, allowable loads, stress intensification factors etc.





# PASS/Equip Nozzle-FEM Advantages



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# Advantages

Key PASS/Equip Nozzle-FEM advantages:

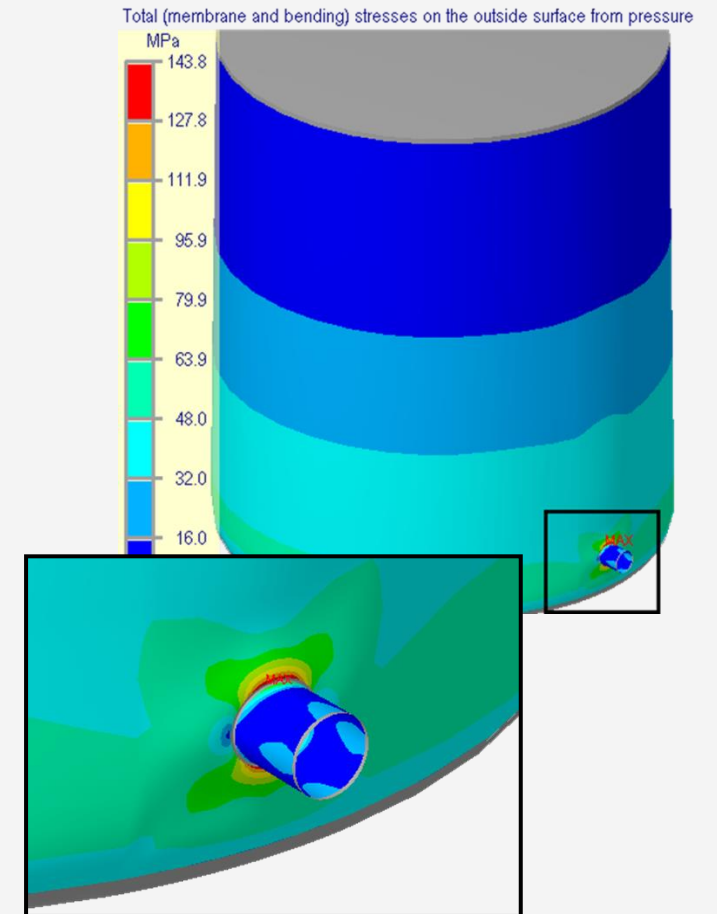
- User friendly modern interface
- Wide range of shell types
- Wide range of nozzle junction types and nozzle placement capabilities
- Different nozzle cross-section shapes
- Affordable price



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# Nozzle-FEM

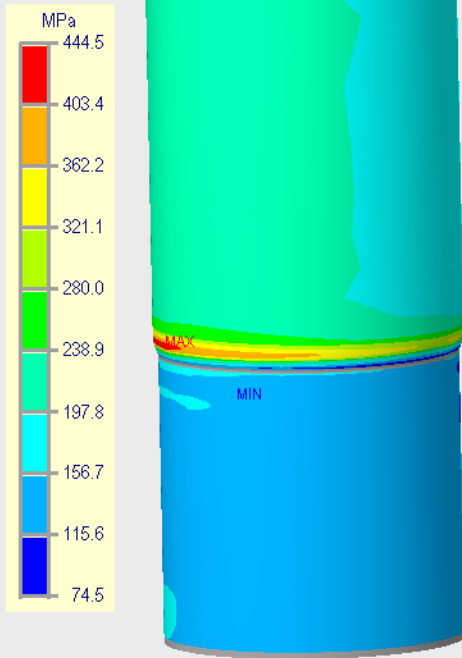
Adding of hydrostatic pressure



# Nozzle-FEM

Connection between skirt  
and vessel (including  
thermal stresses)

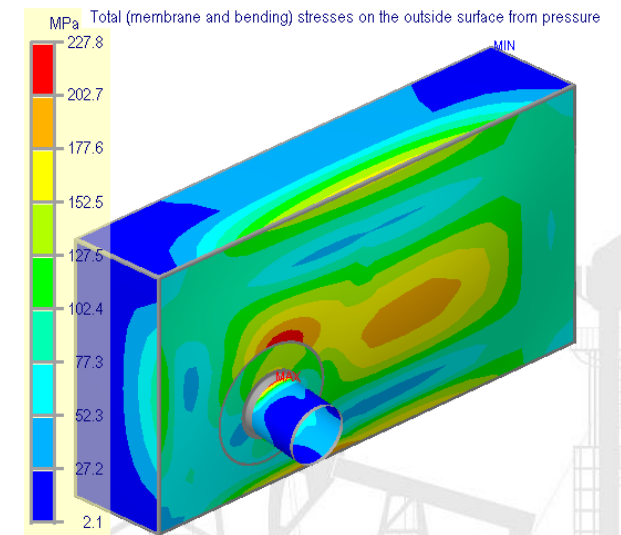
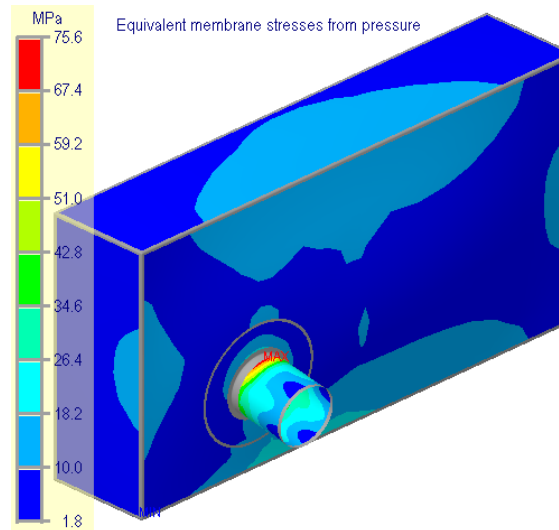
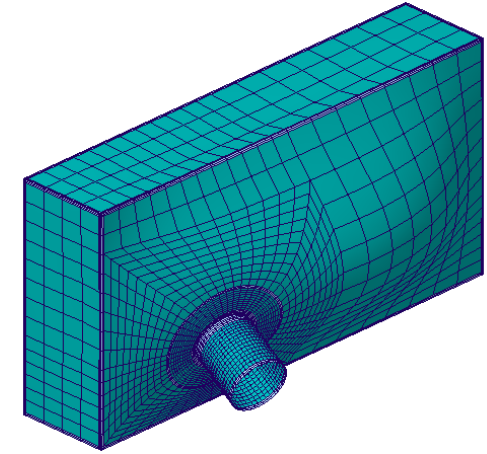
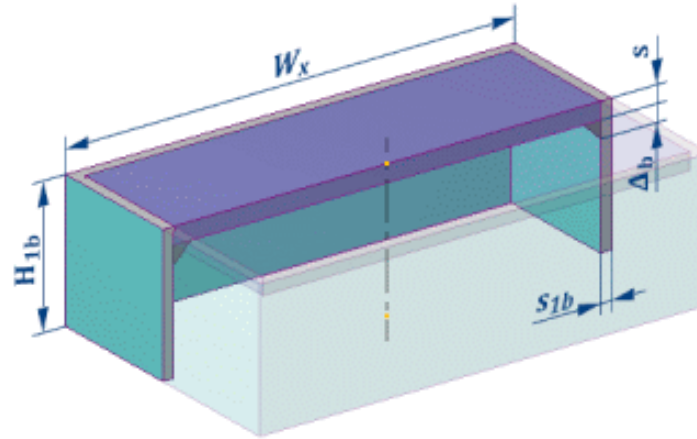
Equivalent membrane stresses from combined action of forces and pressure



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# Examples of advantages

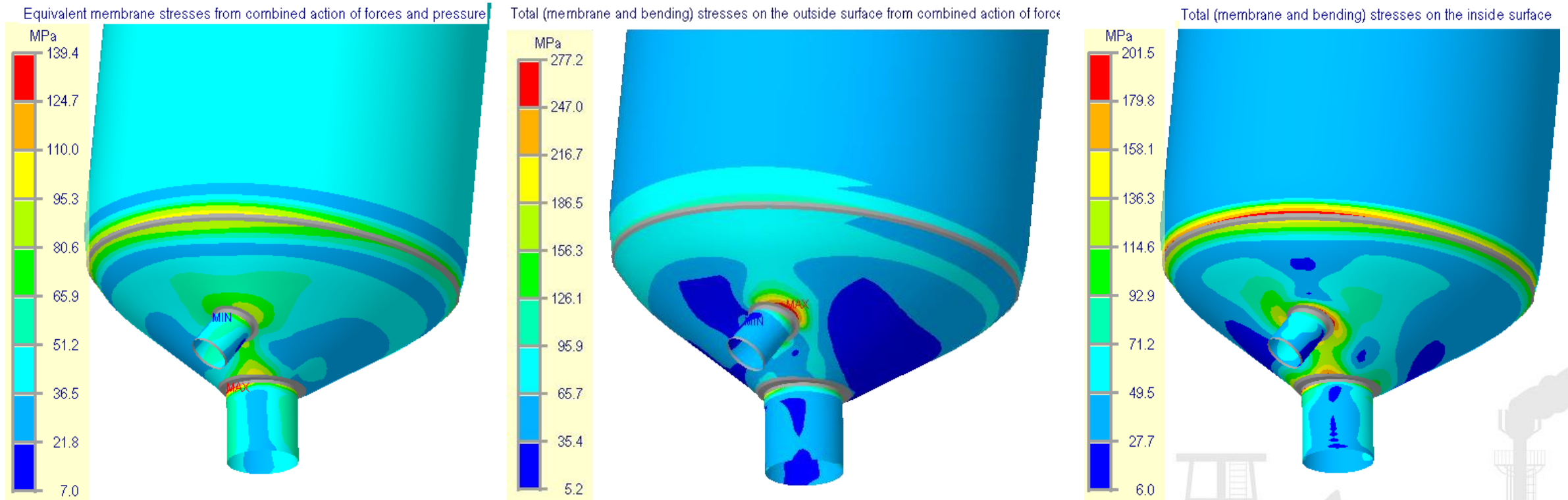
Nozzle in Rectangular Plate



# Examples of advantages | PASS/EQUIP Nozzle-FEM

Conical reducer with two nozzles.

Membrane , membrane + bending stresses (inside, outside)



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THANK YOU!

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